

§ 2 电磁波在半无限绝缘介质分界面上的反射、折射

1. 反射、折射定律

入射角、反射角和折射角的关系；

2. 菲涅耳（Fresnel）公式

入射波、反射波和折射波振幅、位相的关系

3. 布儒斯特（Brewster）定律

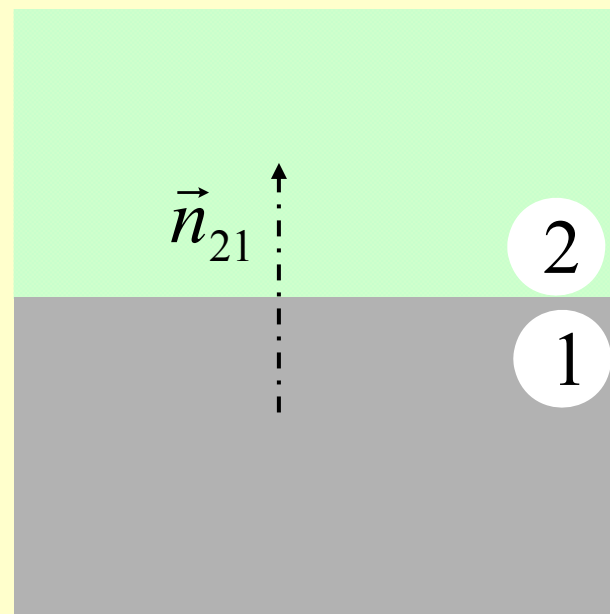
4. 折射、反射系数

5. 全反射现象

1、半无限绝缘介质的分界面上的反射和折射定律

由于是绝缘介质构成的分界面，因此分界面：

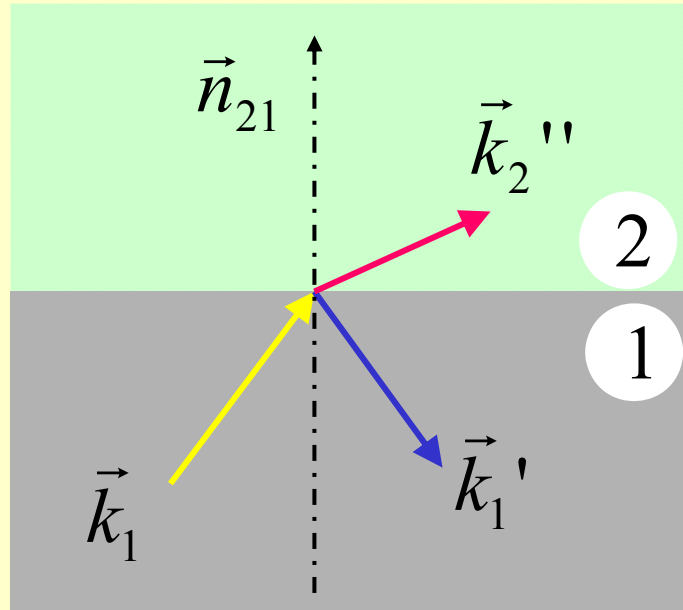
- ① 没有自由电荷面分布
- ② 没有传导电流面分布



$$\begin{array}{l}
 \vec{n}_{21} \cdot (\vec{D}_2 - \vec{D}_1) = 0 \\
 \Rightarrow \vec{n}_{21} \times (\vec{E}_2 - \vec{E}_1) = 0 \\
 \vec{n}_{21} \cdot (\vec{B}_2 - \vec{B}_1) = 0 \\
 \Rightarrow \vec{n}_{21} \times (\vec{H}_2 - \vec{H}_1) = 0
 \end{array}
 \left. \vphantom{\begin{array}{l} \vec{n}_{21} \cdot (\vec{D}_2 - \vec{D}_1) = 0 \\ \vec{n}_{21} \times (\vec{E}_2 - \vec{E}_1) = 0 \\ \vec{n}_{21} \cdot (\vec{B}_2 - \vec{B}_1) = 0 \\ \vec{n}_{21} \times (\vec{H}_2 - \vec{H}_1) = 0 \end{array}} \right\}
 \begin{array}{l}
 \vec{n}_{21} \cdot (\vec{D}_2 - \vec{D}_1) = \sigma_f \\
 \vec{n}_{21} \cdot (\vec{B}_2 - \vec{B}_1) = 0 \\
 \vec{n}_{21} \times (\vec{E}_2 - \vec{E}_1) = 0 \\
 \vec{n}_{21} \times (\vec{H}_2 - \vec{H}_1) = \vec{\alpha}_f
 \end{array}$$

➤ 上述的四个边界条件并非完全独立；

➤ 如果入射波为平面时谐波，则反射波和折射波也为平面时谐波。



入射面：

——入射波矢和面法线构成的面

反射、折射的基本规律：

- ① 反射波、折射波的频率与入射波的频率相等；
- ② 入射线、反射线和折射线处于同一平面（入射面）内；
- ③ 入射角等于反射角；
- ④ 折射线与入射线分布在发界面法线的两侧；
- ⑤ 折射定律：

$$n_1 \sin \theta = n_2 \sin \theta''$$

入射波（平面时谐波）：

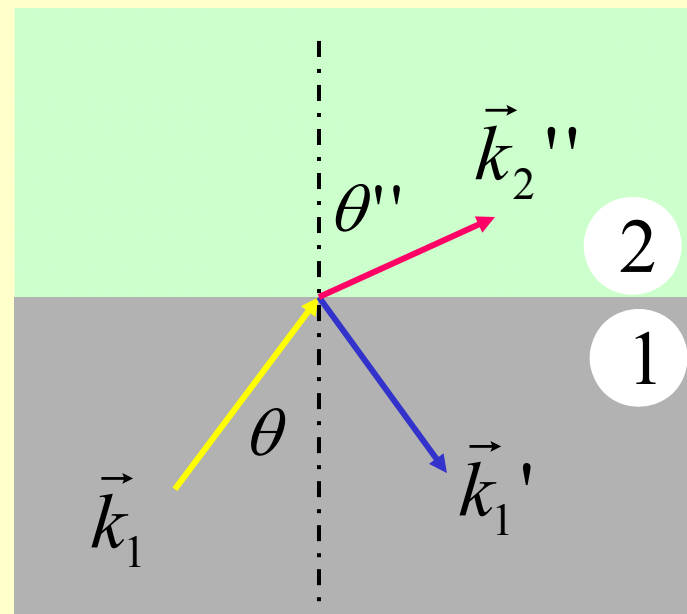
$$\vec{E}(\vec{x}, t) = \vec{E}_0 \exp[i(\vec{k}_1 \cdot \vec{x} - \omega t)]$$

反射波：

$$\vec{E}'(\vec{x}, t) = \vec{E}_0' \exp[i(\vec{k}_1' \cdot \vec{x} - \omega' t)]$$

折射波：

$$\vec{E}''(\vec{x}, t) = \vec{E}_0'' \exp[i(\vec{k}_2'' \cdot \vec{x} - \omega'' t)]$$

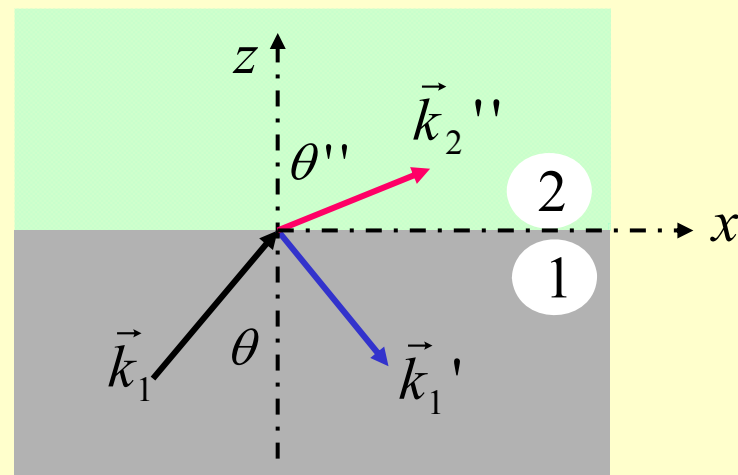


$\vec{n}_{21} \times (\vec{E}_2 - \vec{E}_1) = 0$ 在分界面上的每一点每一时刻都须成立

$$\begin{aligned} \vec{n} \times \vec{E}_0 \exp\left[i(\vec{k}_1 \cdot \vec{x} - \omega t)\right] \Big|_{z=0} + \vec{n} \times \vec{E}_0' \exp\left[i(\vec{k}_1' \cdot \vec{x} - \omega' t)\right] \Big|_{z=0} \\ \equiv \vec{n} \times \vec{E}_0'' \exp\left[i(\vec{k}_2'' \cdot \vec{x} - \omega'' t)\right] \Big|_{z=0} \end{aligned}$$

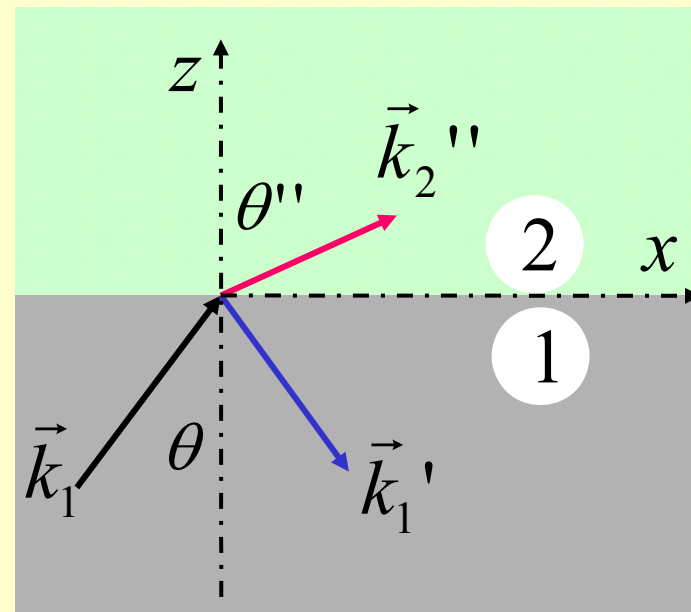
在分界面上， x, y 是两个独立的变量，因此

$$\left\{ \begin{array}{l} \omega = \omega' = \omega'' \\ k_{1x} = k_{1x}' = k_{2x}'' \\ k_{1y} = k_{1y}' = k_{2y}'' \end{array} \right.$$



$k_{1y} = 0$

$k_{1y}' = k_{2y}'' = 0$



反射、折射的基本规律：

- ① 反射波、折射波的频率与入射波的频率相等；
- ② 入射线、反射线和折射线处于同一平面（入射面）内。

$$k_{1x} = k_{1x}' = k_{2x}''$$

根据 $k_{1x} = k_{1x}'$

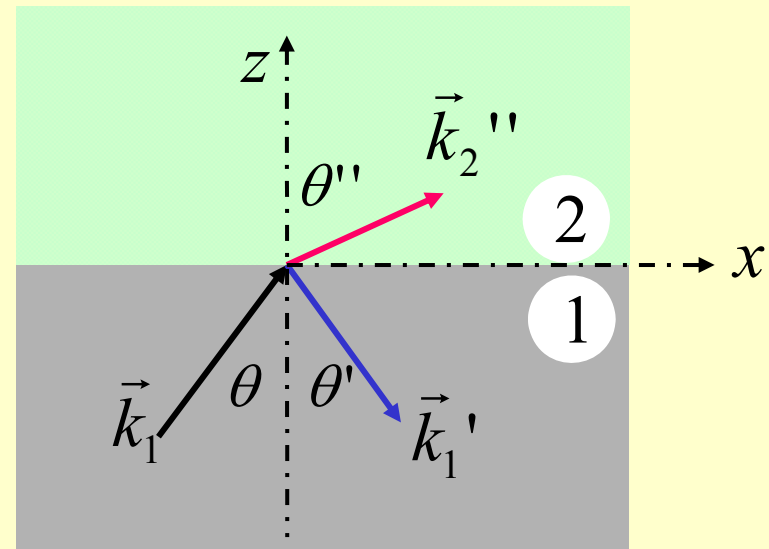
$$k_{1y} = k_{1y}' = k_{2y}''$$

$$k_1 = k_1' = n_1 k$$

得到

$$k_1 \sin \theta = k_1' \sin \theta'$$

或者 $\theta = \theta'$

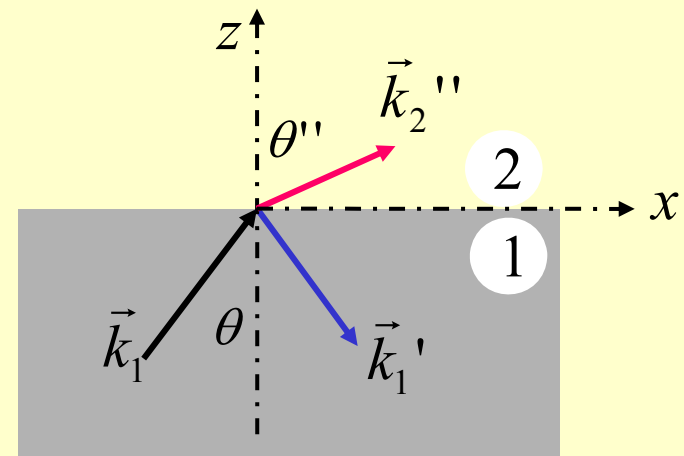


③ 入射角等于反射角。

根据 $k_{1x} = k_{2x}''$

$$k_1 = n_1 k, \quad k_2'' = n_2 k$$

得到: $n_1 \sin \theta = n_2 \sin \theta''$



——光学中的折射定律

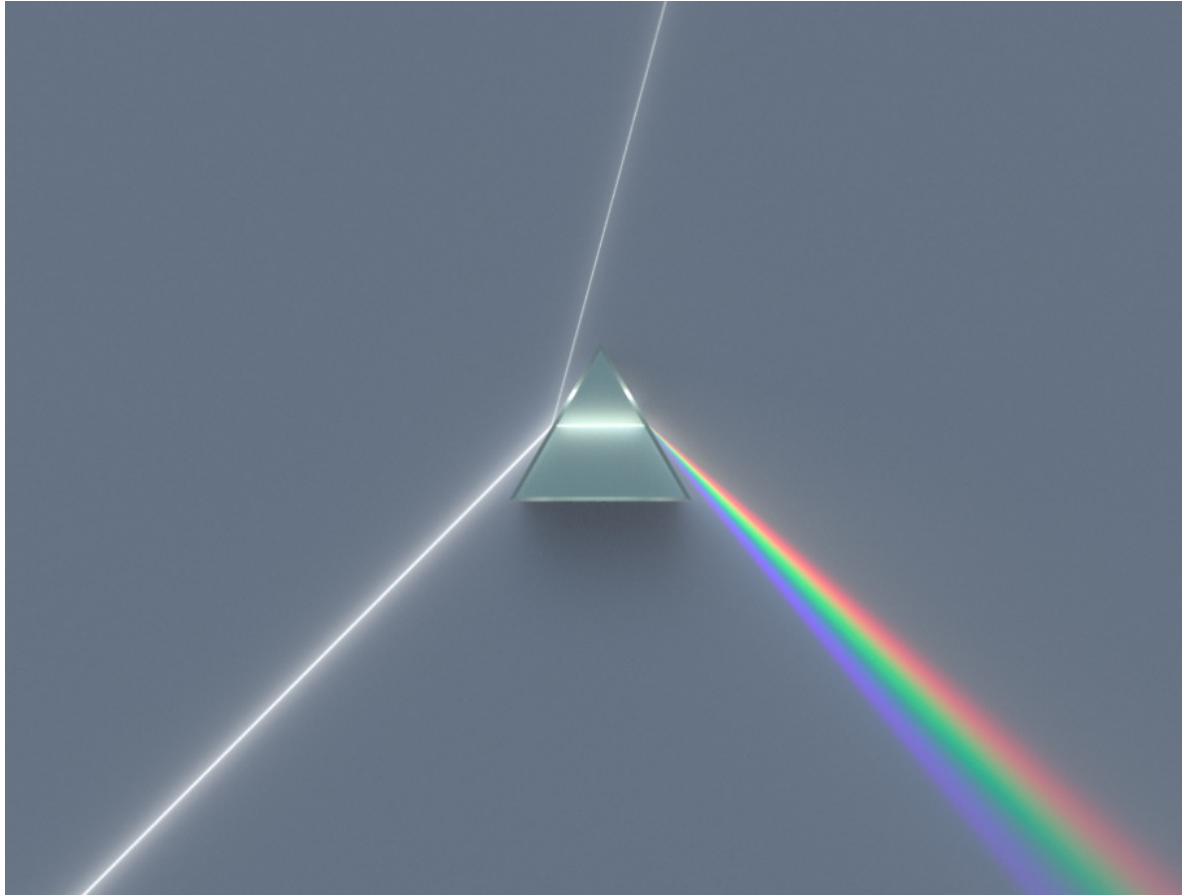
- **折射率**反映了电磁波进入介质时传播方向的折射程度;
- 如果材料(一般是非磁性)的折射率是频率的函数

$$n(\omega) = \sqrt{\mu_r \epsilon_r(\omega)} = \sqrt{\epsilon_r(\omega)}$$

——**介质色散**

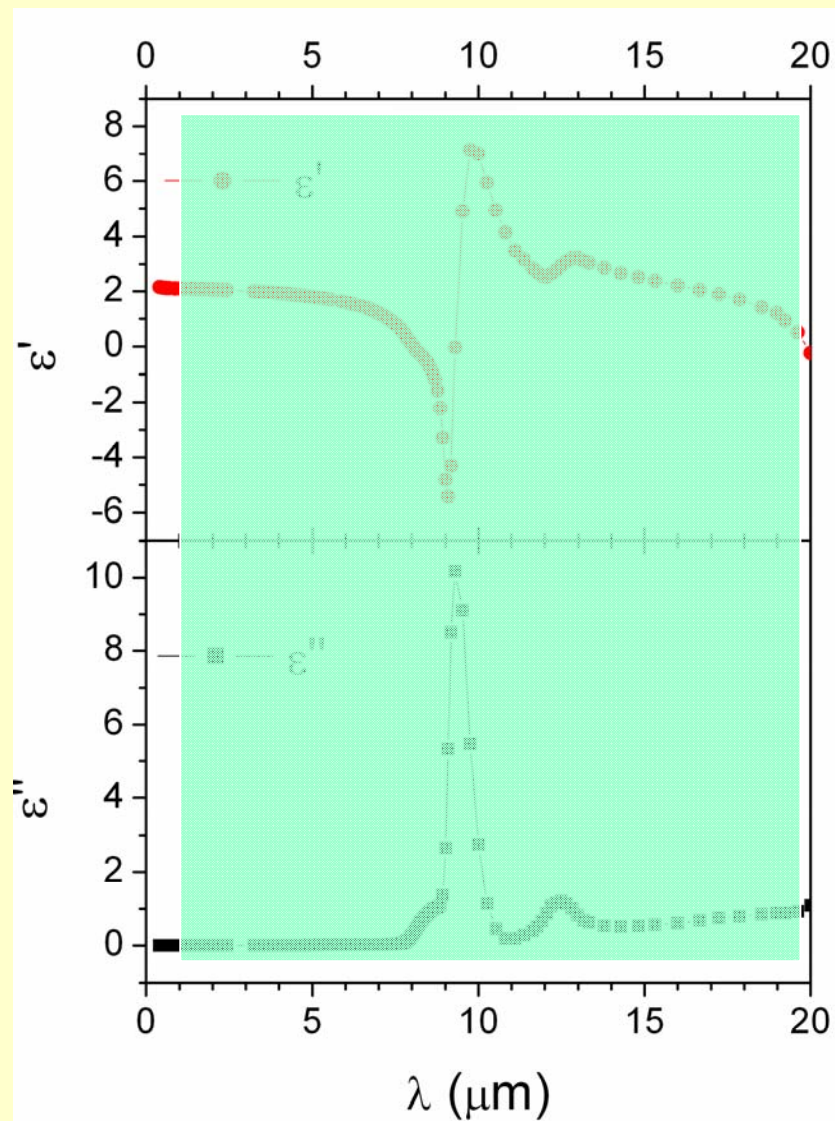
➡ $\theta'' = \theta''(\omega)$

生活中常见光的折射



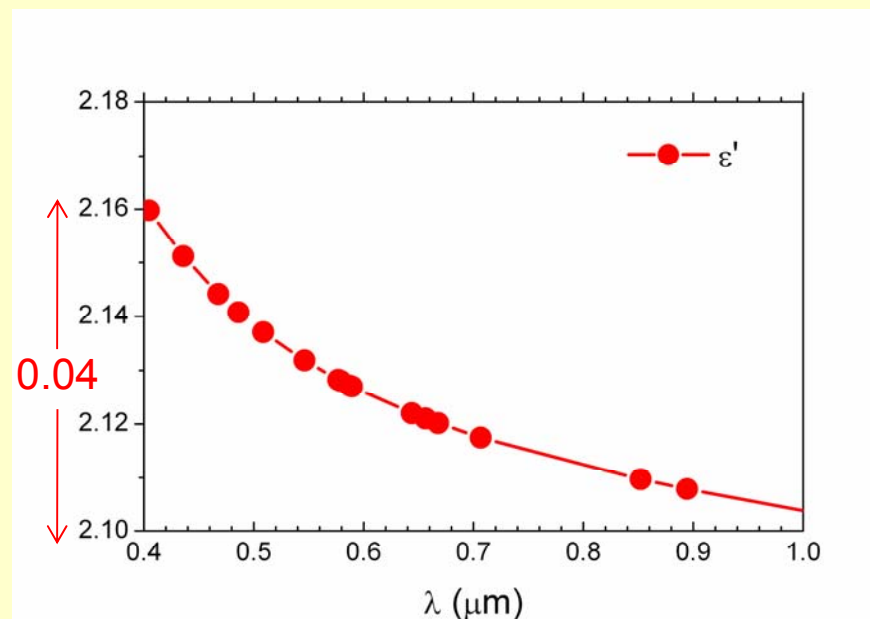
1672年，牛顿用三棱镜将太阳光分解成彩色光带，这是人们首次做的色散实验，说明物质的折射率和光的颜色(波长)有关。

玻璃的介电常数与光波长的关系



$$n = n' + in'' \quad \text{折射率}$$

$$\epsilon = n^2 = \epsilon' + i\epsilon''$$



2、入射波、反射波和折射波的振幅关系

——菲涅耳 (Fresnel) 公式

$$E_{1t} = E_{2t}$$

$$H_{1t} = H_{2t}$$

$$E_{1t} = E_{2t}$$

$$H_{1t} = H_{2t}$$

$$\begin{aligned} \vec{n} \times \vec{E}_0 \exp\left[i(\vec{k}_1 \cdot \vec{x} - \omega t)\right] \Big|_{z=0} + \vec{n} \times \vec{E}_0' \exp\left[i(\vec{k}_1' \cdot \vec{x} - \omega' t)\right] \Big|_{z=0} \\ \equiv \vec{n} \times \vec{E}_0'' \exp\left[i(\vec{k}_2'' \cdot \vec{x} - \omega'' t)\right] \Big|_{z=0} \end{aligned}$$

$$\vec{E}_{0t} + \vec{E}_{0t}' = \vec{E}_{0t}''$$

$$\vec{H}_{0t} + \vec{H}_{0t}' = \vec{H}_{0t}''$$



$$\left\{ \begin{array}{l} \vec{E}_{0t} + \vec{E}'_{0t} = \vec{E}''_{0t} \\ \vec{H}_{0t} + \vec{H}'_{0t} = \vec{H}''_{0t} \end{array} \right.$$

$$\vec{B} = \mu \vec{H}$$

$$|\vec{B}| = \sqrt{\mu \varepsilon} |\vec{E}|$$

$$Z = \sqrt{\frac{\mu}{\varepsilon}}$$

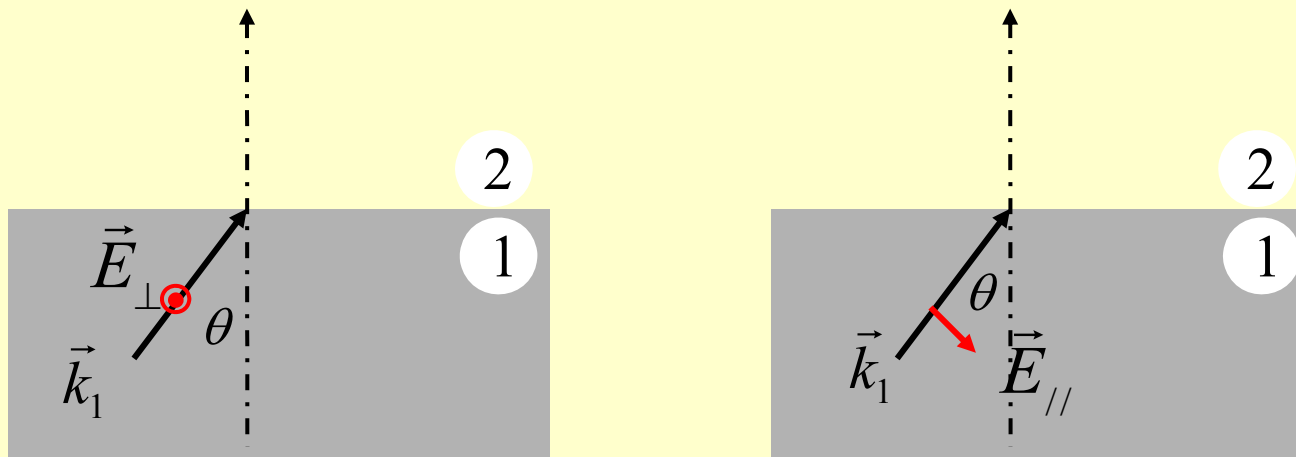
$$|\vec{E}| = Z |\vec{H}|$$

➤ 对于给定的波矢，电场存在两个独立的振动（偏振）方向；

➤ 为讨论方便，将电场矢量分解为

① 偏振方向垂直于入射面(S-polarization) (\vec{E}_\perp)

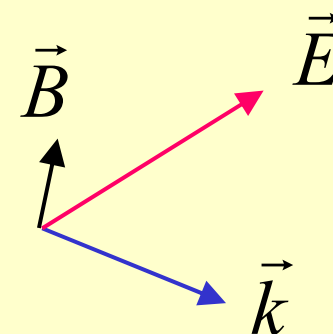
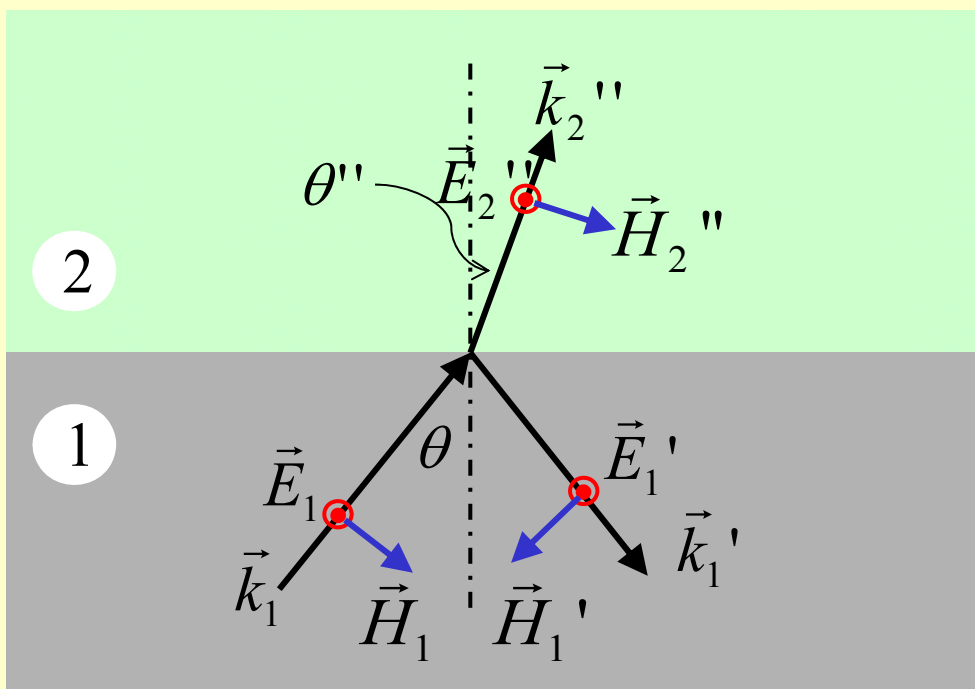
② 偏振方向处于入射面内(P-polarization) (\vec{E}_\parallel)



一般的情况下， $\vec{E} = \vec{E}_\parallel + \vec{E}_\perp$

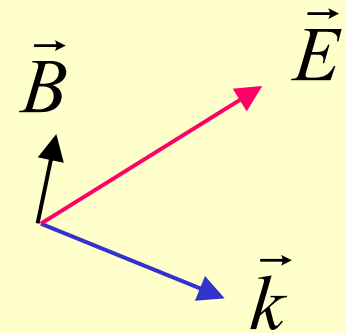
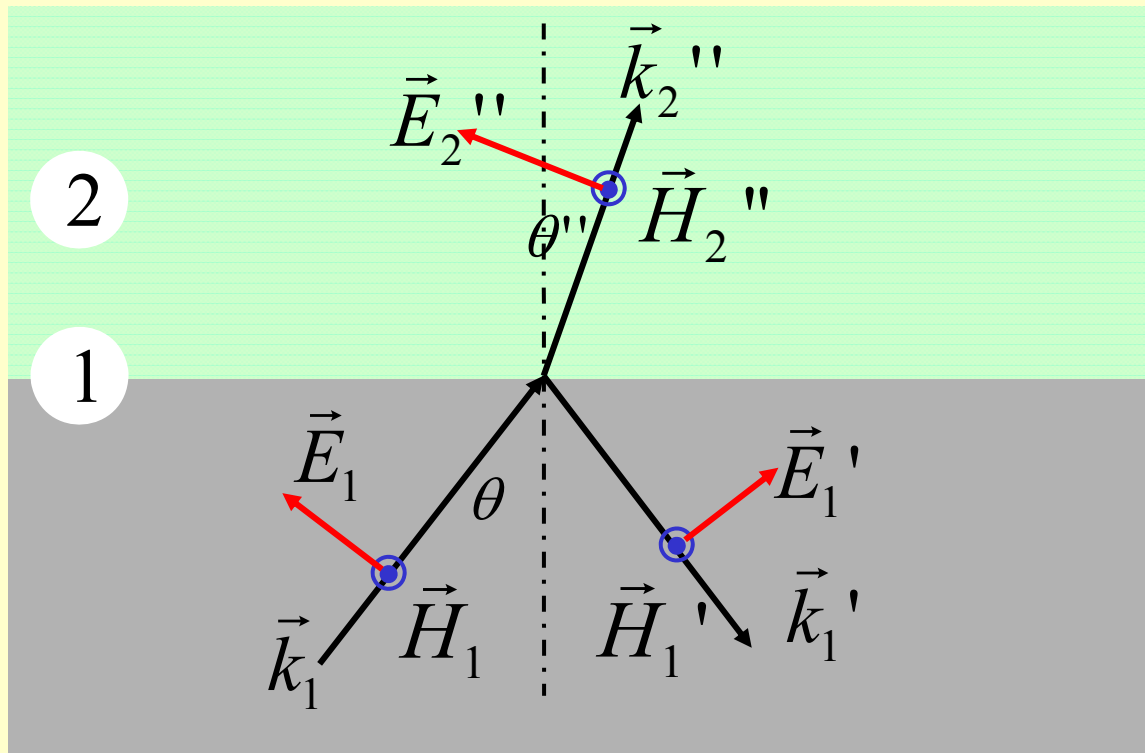
(1) 偏振方向垂直于入射面 (S-polarization)

(选取垂直版面向外, 作为电场的正方向)

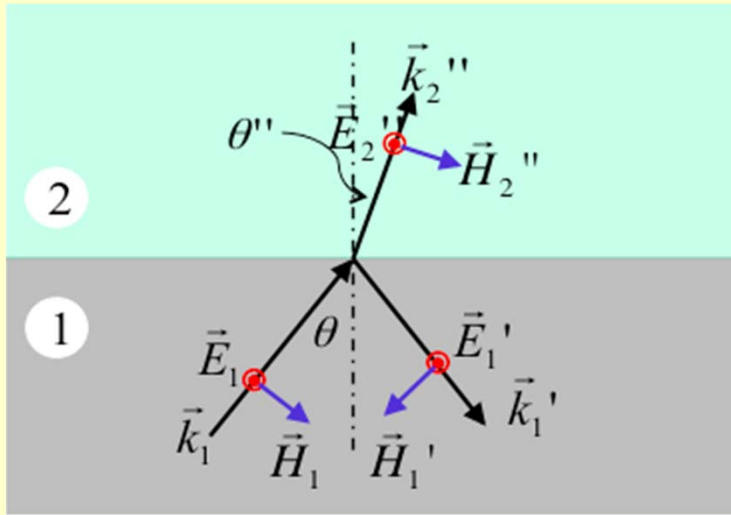


(2) 偏振方向平行于入射面 (P-polarization)

(选取垂直版面向外, 作为磁感应强度的正方向)



(1) 偏振方向垂直于入射面 (S-polarization)



$$\vec{E}_{0t} + \vec{E}_{0t}' = \vec{E}_{0t}''$$

$$\vec{H}_{0t} + \vec{H}_{0t}' = \vec{H}_{0t}''$$



$$E_0 + E_0' = E_0''$$

$$H_1 \cos \theta - H_1' \cos \theta = H_2'' \cos \theta''$$



$$\frac{1}{Z_1} [E_0 \cos \theta - E_0' \cos \theta] = \frac{1}{Z_2} E_0'' \cos \theta''$$

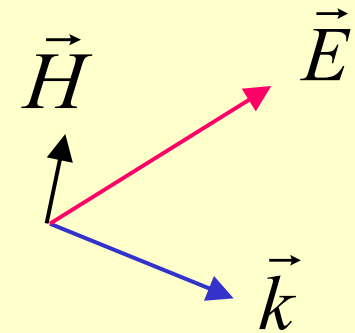
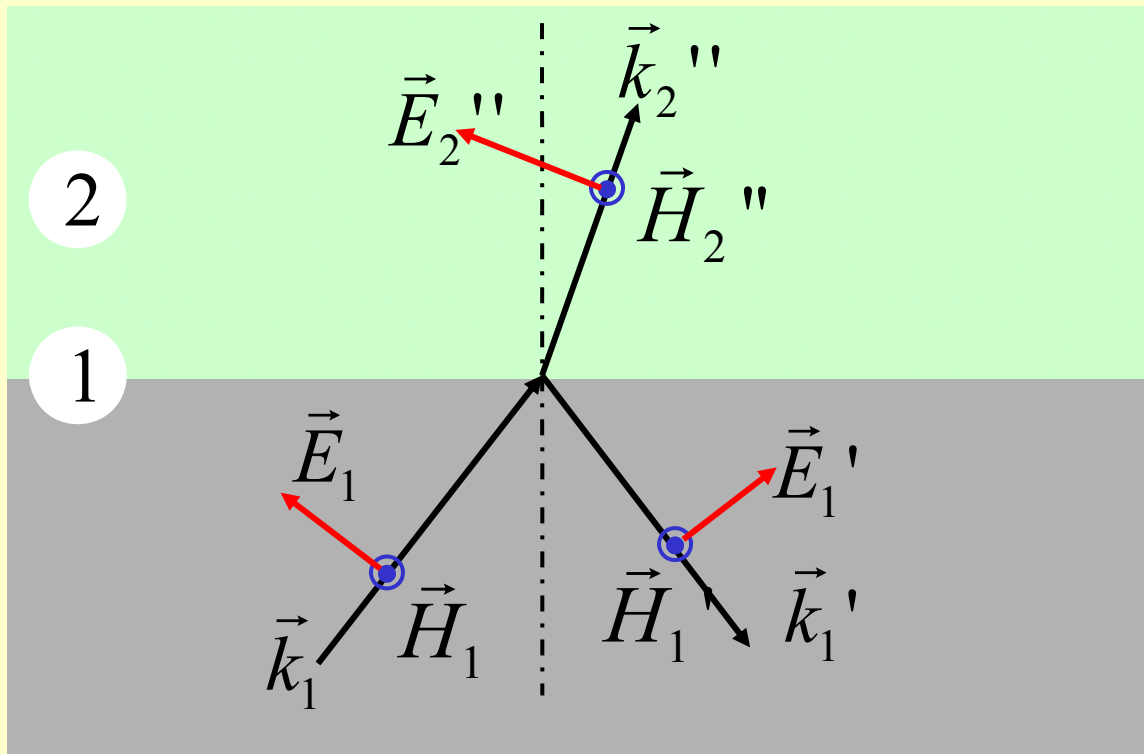
$$E_0 + E_0' = E_0''$$

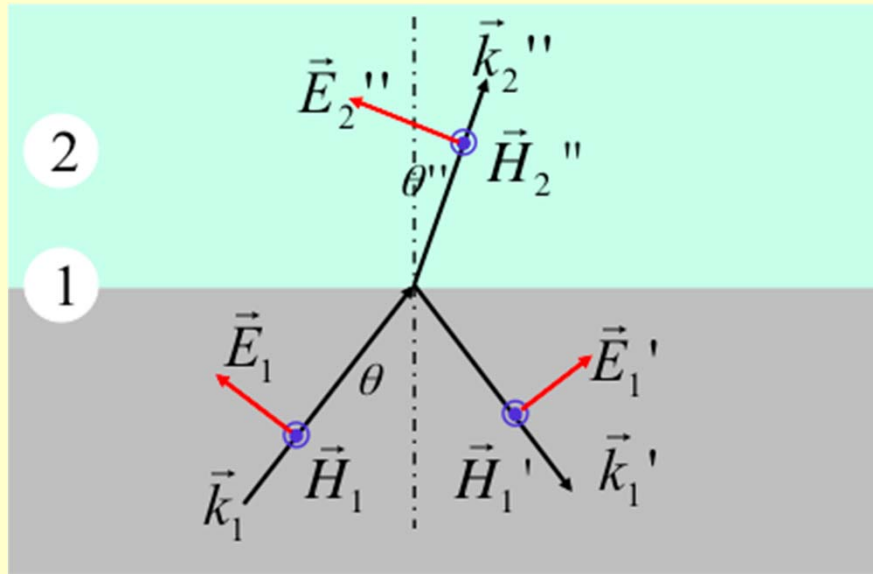
$$\frac{1}{Z_1} [E_0 \cos \theta - E_0' \cos \theta] = \frac{1}{Z_2} E_0'' \cos \theta$$

S偏振入射下的反射波：
$$\frac{E_0'}{E_0} = \frac{Z_2 \cos \theta - Z_1 \cos \theta}{Z_2 \cos \theta + Z_1 \cos \theta}$$

S偏振入射下的透射波：
$$\frac{E_0''}{E_0} = \frac{2Z_2 \cos \theta}{Z_2 \cos \theta + Z_1 \cos \theta}$$

(2) 偏振方向平行于入射面 (P-polarization)





$$\vec{E}_{0t} + \vec{E}_{0t}' = \vec{E}_{0t}''$$

$$\vec{H}_{0t} + \vec{H}_{0t}' = \vec{H}_{0t}''$$

→ $H_0 + H_0' = H_0''$

$$-E_0 \cos \theta + E_0' \cos \theta' = -E_0'' \cos \theta''$$

$$Z_1(-H_0 \cos \theta + H_0' \cos \theta') = -Z_2 H_0'' \cos \theta''$$

→ $\frac{1}{Z_2}(-H_0 \cos \theta + H_0' \cos \theta') = -\frac{1}{Z_1} H_0'' \cos \theta''$

求解得：

P偏振入射下的反射波

$$\frac{H_0'}{H_0} = \frac{-Z_1 \cos \theta + Z_2 \cos \theta''}{Z_1 \cos \theta + Z_2 \cos \theta''}$$

P偏振入射下的透射波

$$\frac{H_0''}{H_0} = \frac{2Z_2 \cos \theta''}{Z_1 \cos \theta + Z_2 \cos \theta''}$$

归纳如下：

反射波

$$\text{(s-polar.) } \frac{E_0'}{E_0} = \frac{Z_2 \cos \theta - Z_1 \cos \theta''}{Z_2 \cos \theta + Z_1 \cos \theta''}$$

$$\text{(p-polar.) } \frac{H_0'}{H_0} = \frac{-Z_1 \cos \theta + Z_2 \cos \theta''}{Z_1 \cos \theta + Z_2 \cos \theta''}$$

折射波

$$\frac{E_0''}{E_0} = \frac{2Z_2 \cos \theta}{Z_2 \cos \theta + Z_1 \cos \theta''}$$

$$\frac{H_0''}{H_0} = \frac{2Z_2 \cos \theta''}{Z_1 \cos \theta + Z_2 \cos \theta''}$$

讨论：1) 在垂直入射下：

$$\frac{E_0'}{E_0} = \frac{Z_2 - Z_1}{Z_2 + Z_1}$$

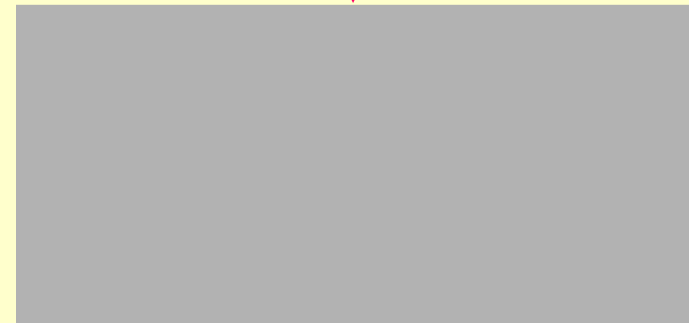
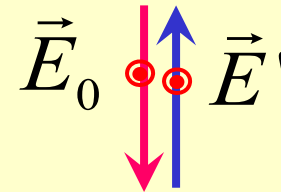
假设电磁波从真空入射到
相对阻抗 Z_r 的介质表面：

$$\frac{E_0'}{E_0} = \frac{Z_r - 1}{Z_r + 1} \left(Z_r = \sqrt{\frac{\mu_r}{\epsilon_r}} \right)$$

- 阻抗描述了电磁波入射到分界面时的振幅的比值（包括位相）关系；
- 在 $\epsilon_r \rightarrow -\infty$ （理想导体）或 $\mu_r \rightarrow -\infty$ （理想磁导体），都能够产生强烈的反射。

$$\frac{E_0'}{E_0} = \frac{Z_2 \cos \theta - Z_1 \cos \theta''}{Z_2 \cos \theta + Z_1 \cos \theta''}$$

(S polar.)



2) 对于**非磁性介质**， $\mu_1 = \mu_2 = \mu_0$ 的情况下，
上述公式学过度到光学中的菲涅耳公式：

反射波

折射波

(s-polar.)
$$\frac{E_{0\perp}'}{E_{0\perp}} = \frac{\sin(\theta'' - \theta)}{\sin(\theta'' + \theta)}$$

$$\frac{E_{0\perp}''}{E_{0\perp}} = \frac{2 \cos \theta \sin \theta''}{\sin(\theta'' + \theta)}$$

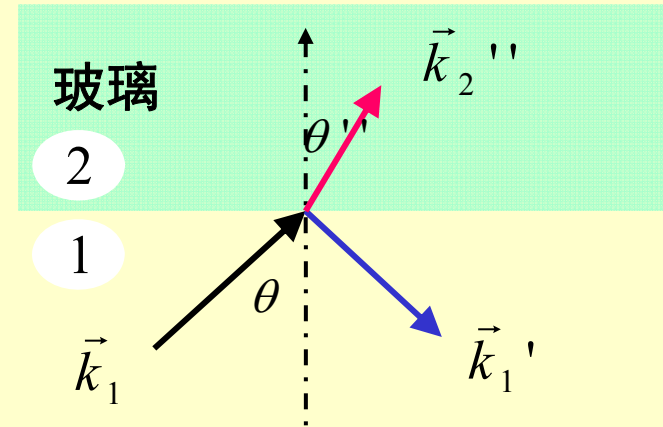
(p-polar.)
$$\frac{E_{0\parallel}'}{E_{0\parallel}} = \frac{\tan(\theta - \theta'')}{\tan(\theta + \theta'')}$$

$$\frac{E_{0\parallel}''}{E_{0\parallel}} = \frac{2 \cos \theta \sin \theta''}{\sin(\theta'' + \theta) \cos(\theta - \theta'')}$$

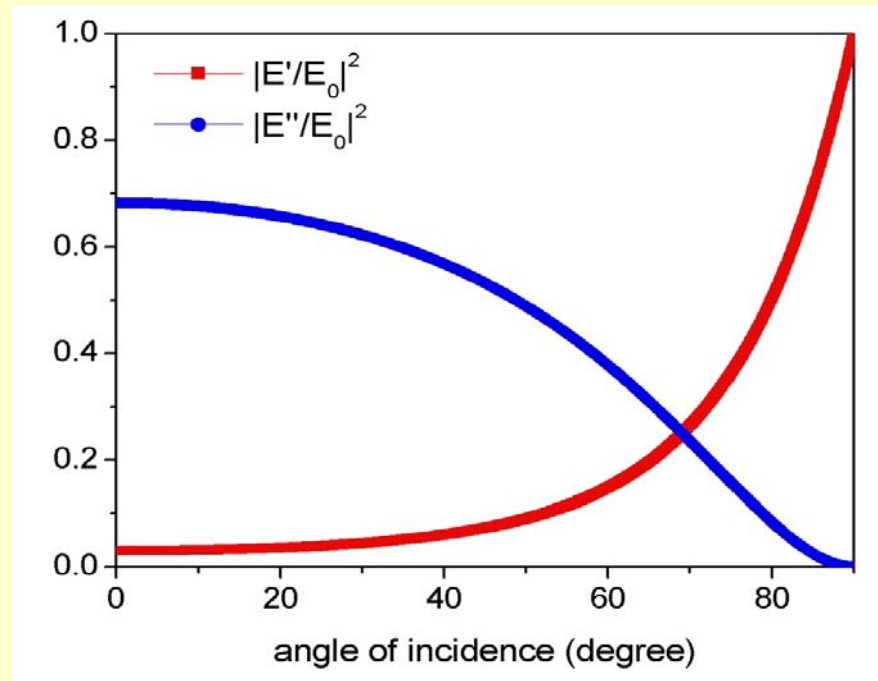
待继续

3) 斜入射下情形:

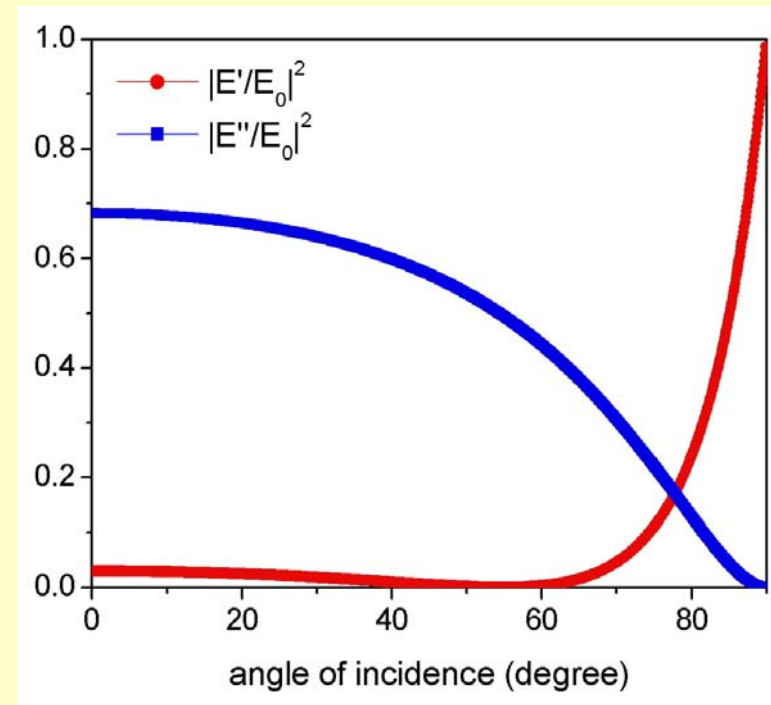
假设: ($n_1 = 1.00$, $n_2 = 1.42$)



S-偏振入射:



p-偏振入射:

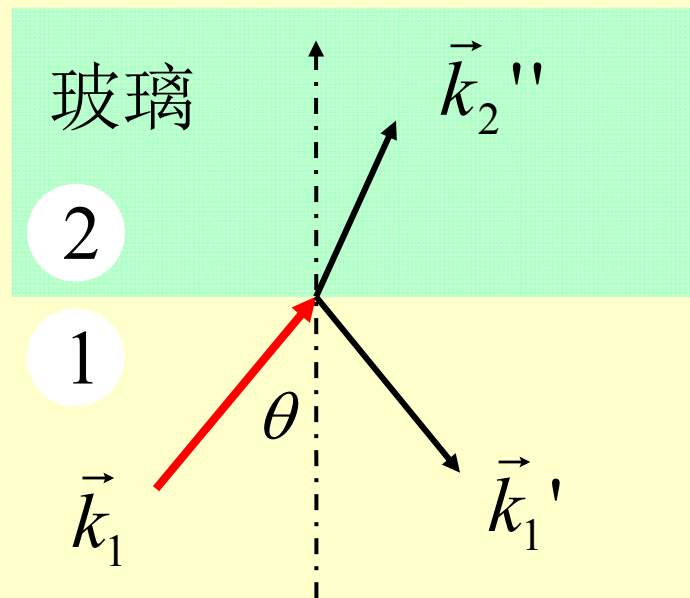


结论：

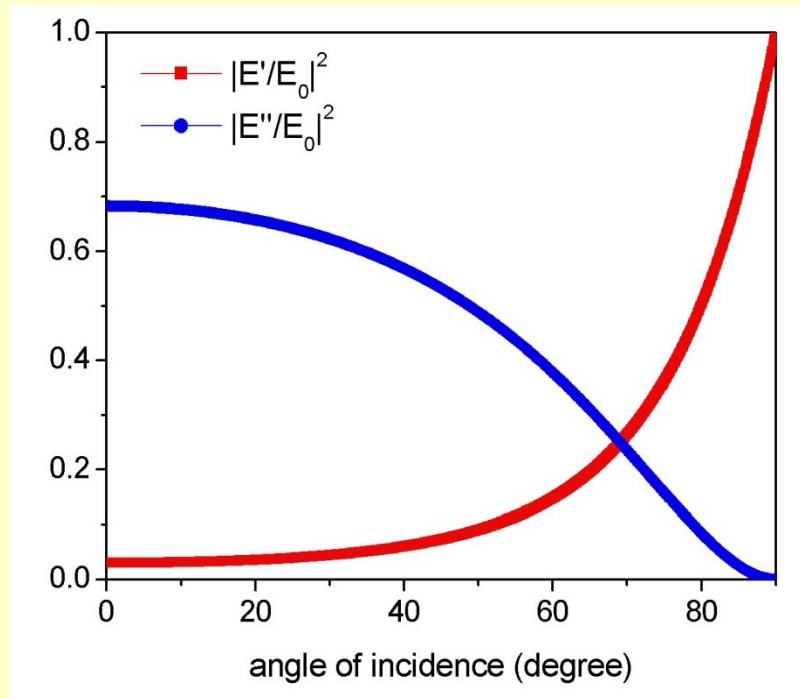
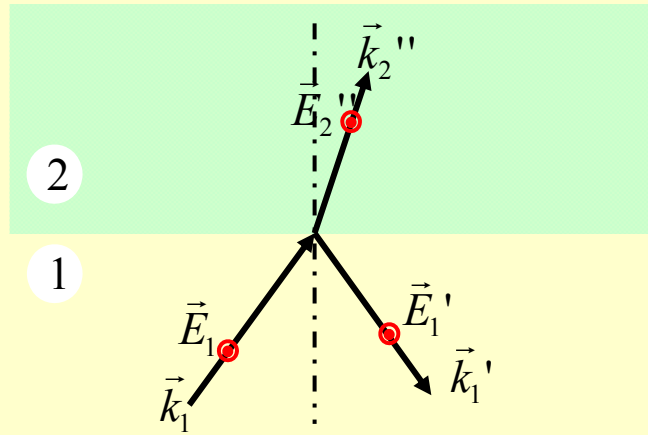
- ① 偏振方向垂直于入射面的光波反射、折射行为不完全等同于偏振平行于入射面的光波的反射和折射行为；
- ② 如果入射光为自然光（两种偏振的等量混合），经过反射（折射）后，由于两个偏振的反射（折射）强度不同，反射光（折射光）变成了部分偏振光；

3、布儒斯特 (Brewster) 定律

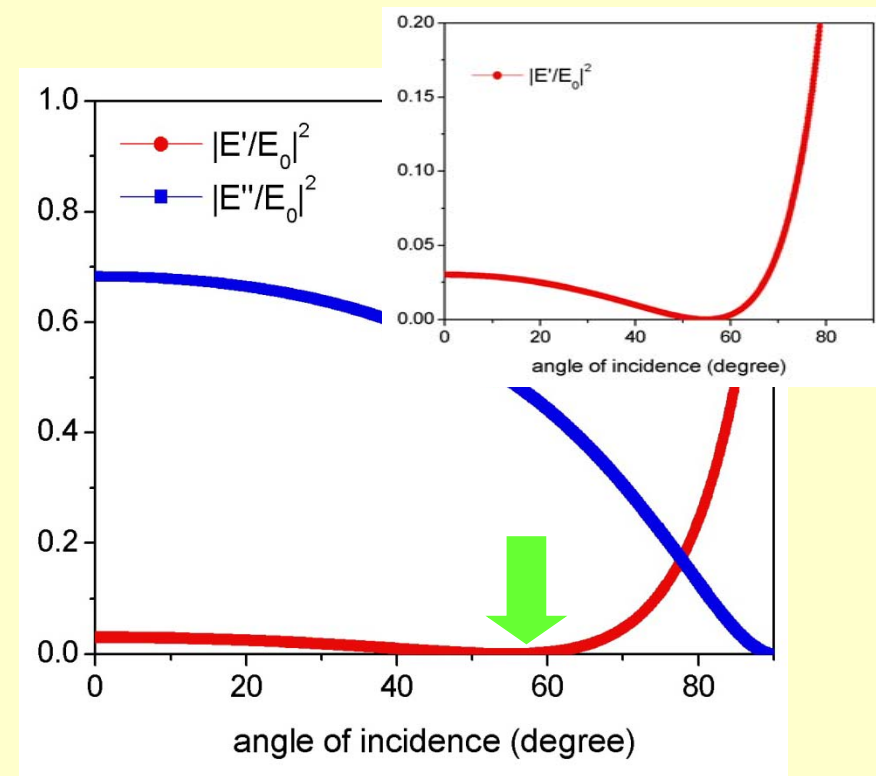
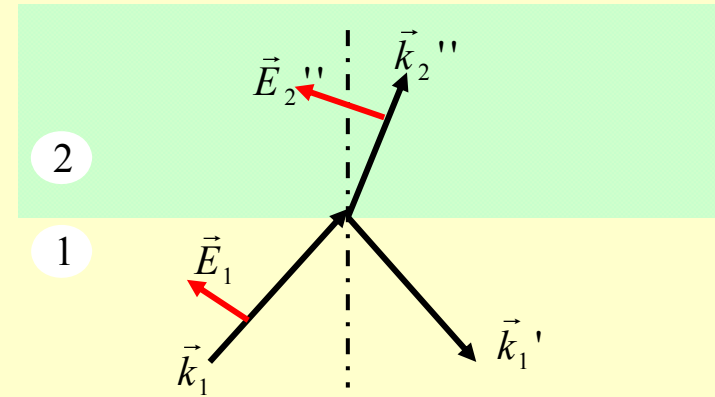
假设： $n_1 = 1.00$, $n_2 = 1.42$



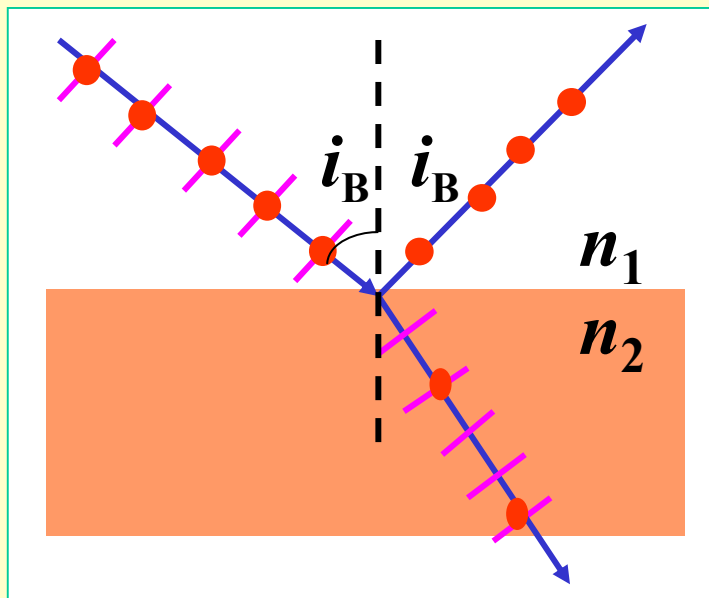
s-polarization



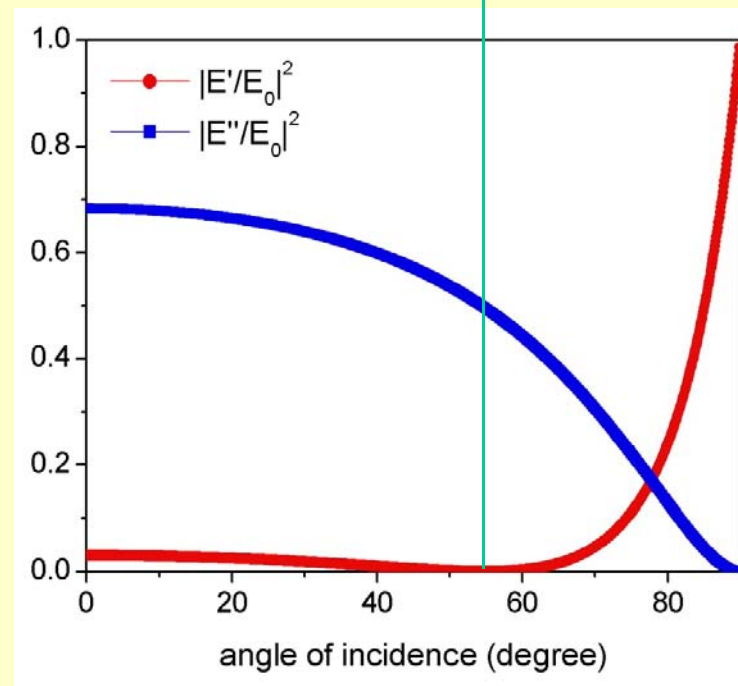
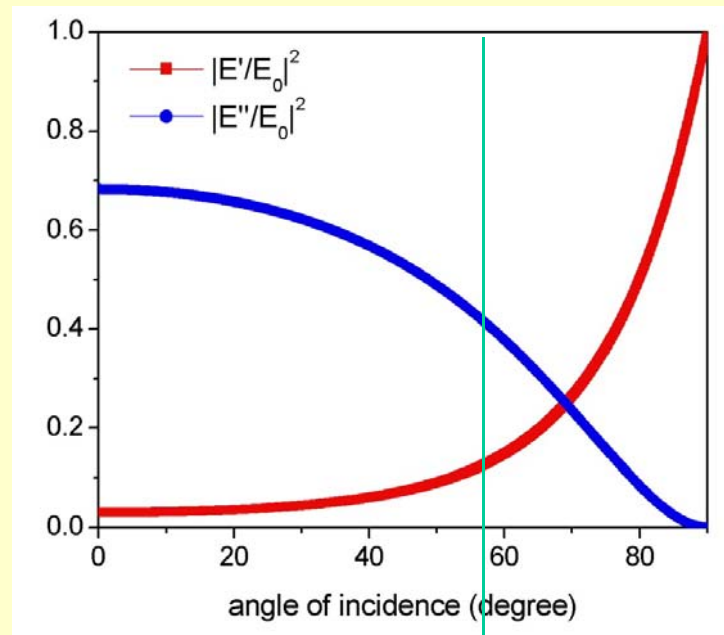
p-polarization



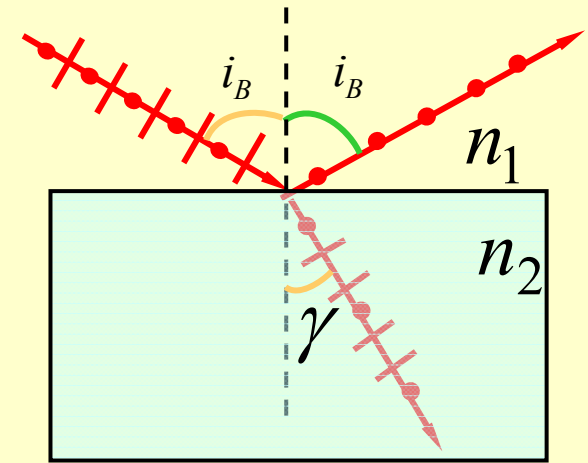
入射角度为布儒斯特角，含有两种偏振状态（P偏振的反射率为零！）



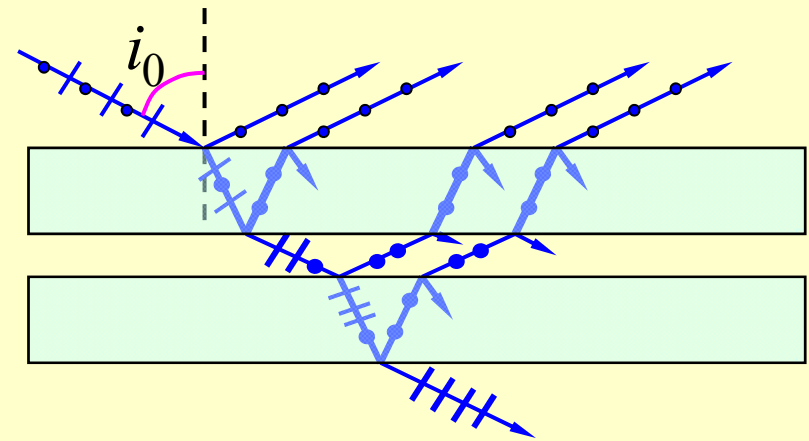
反射光：虽为纯的S偏振的线偏振，但反射率比较低，应用价值不大！



- 在入射角等于布儒斯特角时，在反射光中只有一种（S）偏振。



- 一般光学玻璃反射光的强度约占入射光强度的7.5%，大部分光将透过玻璃。



垂直振动**S**成分一次次被反射掉，折射光：近似线偏振光(**P**偏振)

p-polarization:

$$\frac{E_{0//}'}{E_{0//}} = \frac{\tan(\theta - \theta'')}{\tan(\theta + \theta'')}$$

在 $\theta + \theta'' = 90^\circ$ 的特殊情况下, $E_{0//}' = 0$ 。

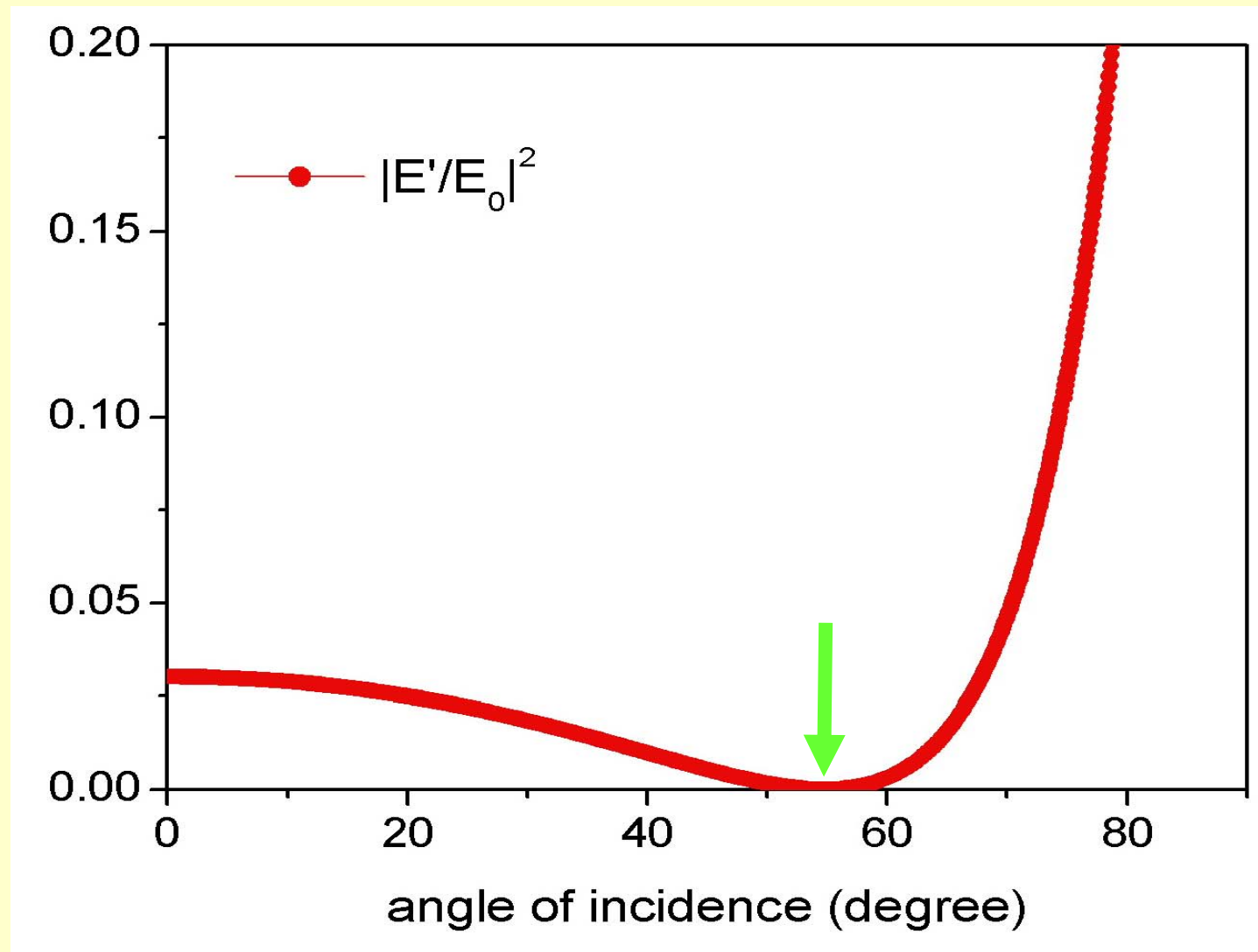
布儒斯特角:

$$n_1 \sin \theta = n_2 \sin \theta''$$

$$n_1 \sin \theta_B = n_2 \sin(90^\circ - \theta_B) = n_2 \cos \theta_B$$

$$\tan \theta_B = \frac{n_2}{n_1}, \quad \theta_B = \arctan \frac{n_2}{n_1}$$

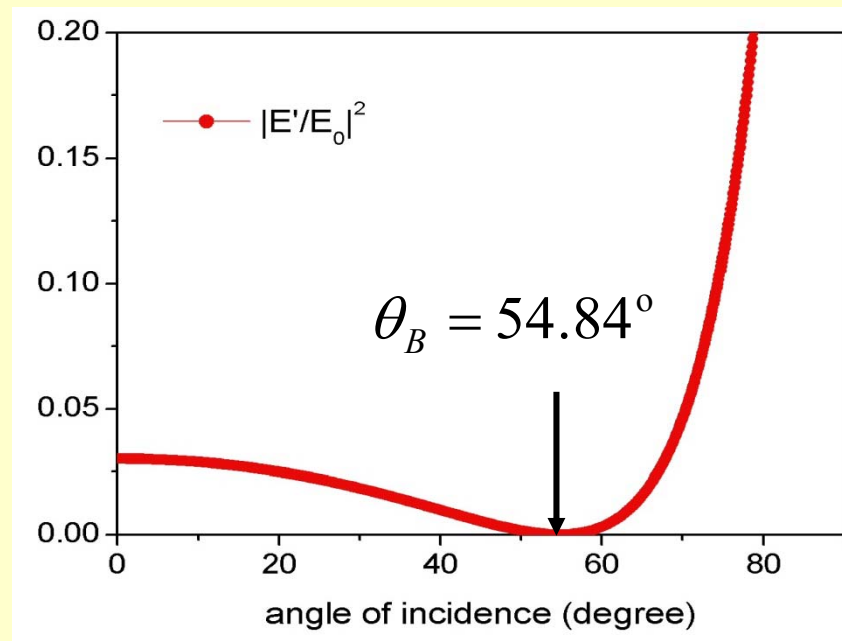
p-polarization



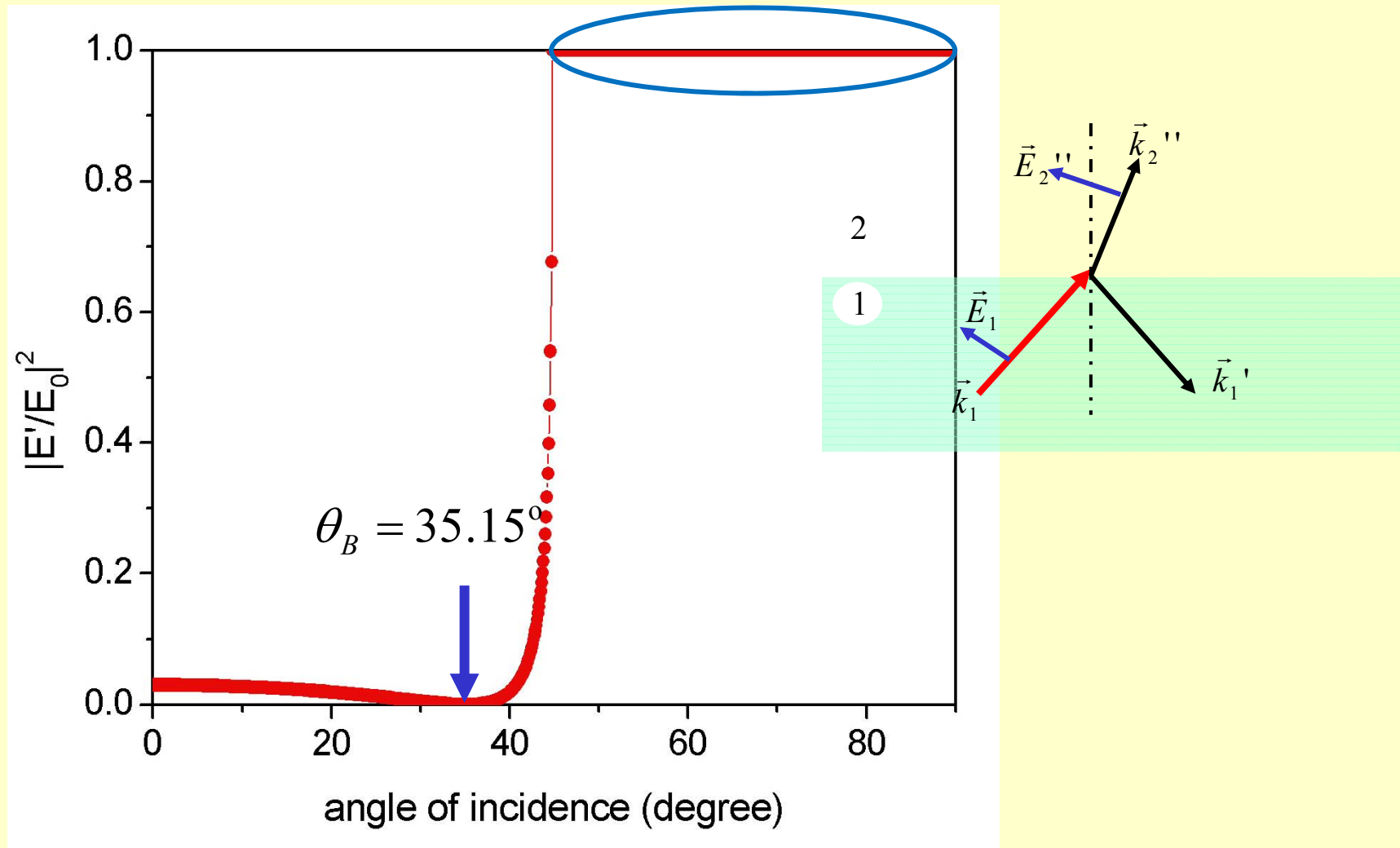
$$\tan \theta_B = \frac{n_2}{n_1}, \quad \theta_B = \arctan \frac{n_2}{n_1}$$

假设: $n_1 = 1.00$, $n_2 = 1.42$

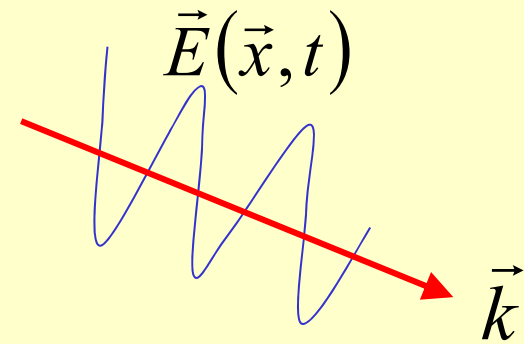
$$\theta_B = \arctan \frac{n_2}{n_1} = \arctan 1.42 = 54.84^\circ$$



如果: $n_1 = 1.42$, $n_2 = 1.00$ $\theta_B = \arctan \frac{1}{1.42} = 35.15^\circ$



4、介质分界面的折射系数、反射系数



平面电磁波的平均能流密度：

$$\langle \vec{S} \rangle = \frac{1}{2} \sqrt{\frac{\epsilon}{\mu}} E_0^2 \vec{e}_k$$

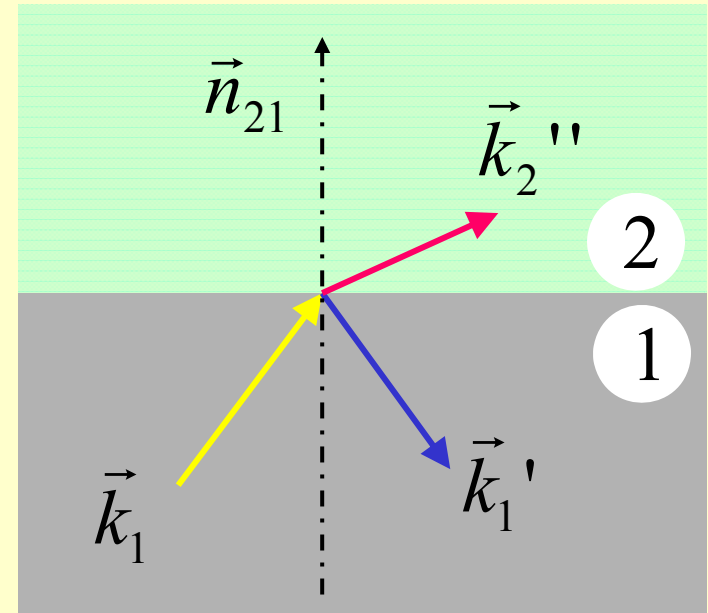
$$\langle \vec{S} \rangle = \frac{1}{2} \sqrt{\frac{\epsilon}{\mu}} E_0^2 \vec{e}_k = \frac{1}{2} Z^{-1} E_0^2 \vec{e}_k$$

1) 反射波的平均能流密度

$$\langle \vec{S}' \rangle = \frac{1}{2} Z_1^{-1} |E_0'|^2 \vec{e}_{k'}$$

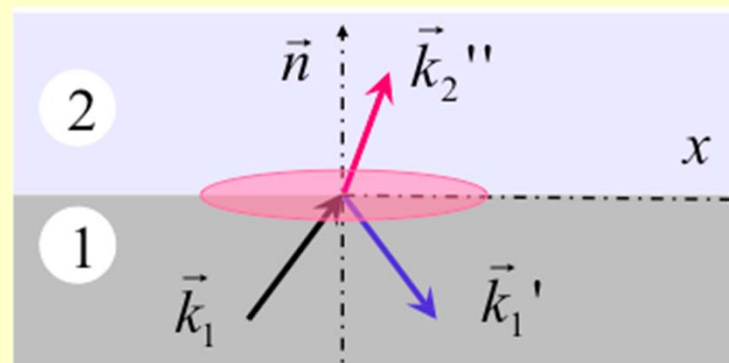
2) 折射波的平均能流密度

$$\langle \vec{S}'' \rangle = \frac{1}{2} Z_2^{-1} |E_0''|^2 \vec{e}_{k''}$$



3) 反射系数:

$$R = \frac{\langle \vec{S}' \rangle \cdot \vec{n}}{\langle \vec{S} \rangle \cdot \vec{n}} = \frac{|E_0'|^2 \vec{e}_{k'} \cdot \vec{n}}{|E_0|^2 \vec{e}_k \cdot \vec{n}} = \frac{|E_0'|^2}{|E_0|^2}$$



4) 折射系数:

$$T = \frac{\langle \vec{S}'' \rangle \cdot \vec{n}}{\langle \vec{S} \rangle \cdot \vec{n}} = \frac{Z_2^{-1} |E_0''|^2 \vec{e}_{k''} \cdot \vec{n}}{Z_1^{-1} |E_0|^2 \vec{e}_k \cdot \vec{n}} = \frac{Z_2^{-1} |E_0''|^2 \cos \theta''}{Z_1^{-1} |E_0|^2 \cos \theta}$$

注意:

定义反射/透射率的时候, 不是直接对入(反、透)射波的能量流的比值, 而是考虑这些能流对界面的通量。

Insect orientation to polarized moonlight

- Sunlight scatters when it strikes tiny particles in the atmosphere, giving rise to **celestial polarization** patterns
- Many creatures use the **Sun's light-polarization pattern** to orientate themselves

Insect orientation to polarized moonlight

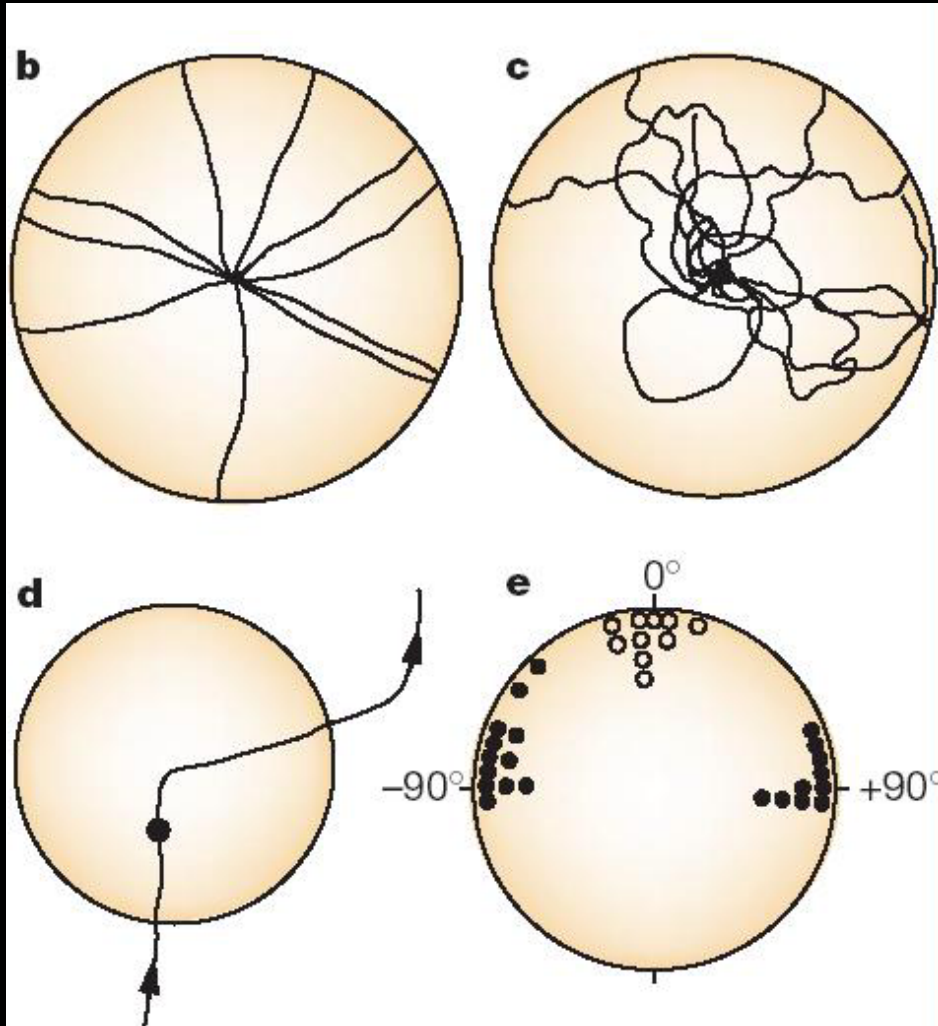


An African dung beetle uses **the moonlit sky** to make a swift exit after finding food.

The beetle is rolling a ball of dung.

M. Dacke *et al.* *Nature* **424** (2003) 33

Paths taken by beetles ($n = 10$) moving dung balls outwards from the centre of an arena (diameter, 3 m).



- b) On a moonlit night
- c) On moonless nights
- d) Change in direction (turn to the right by $+70^\circ$) taken by a beetle when a perpendicularly polarizing filter is placed over the beetle at the point indicated by the dot; the beetle resumes its direction of travel on exposure to the open sky.

Polarized light as a butterfly mating signal



This optical feature of some iridescent wings catches a suitor's eye in the deep forest.

A. Sweeney *et al.*
Nature **424** (2003) 31

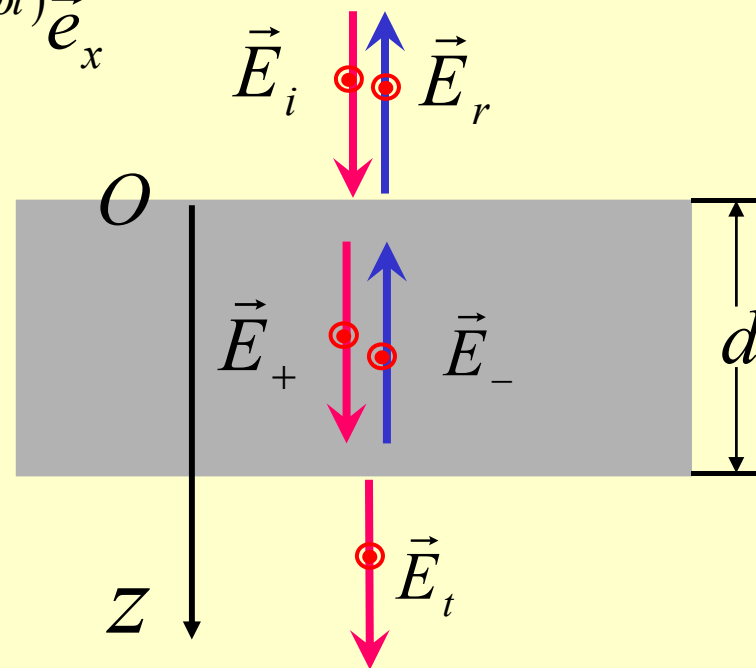
思考题：单色平面电磁波垂直入射到一介质膜上，在入射区，存在入射和反射波；在介质膜内，存在前向和反向波；在透射区存在透射波，分别表示为

$$\vec{E}_i = E_{i0} e^{i(kz - \omega t)} \vec{e}_x, \quad \vec{E}_r = E_{r0} e^{i(-kz - \omega t)} \vec{e}_x$$

$$\vec{E}_+ = E_{+0} e^{i(k_m z - \omega t)} \vec{e}_x$$

$$\vec{E}_- = E_{-0} e^{i(-k_m z - \omega t)} \vec{e}_x$$

$$\vec{E}_t = E_{t0} e^{i(kz - \omega t)} \vec{e}_x$$



根据介质分界面处电磁场边界条件，写出上述电场振幅之间的关系。

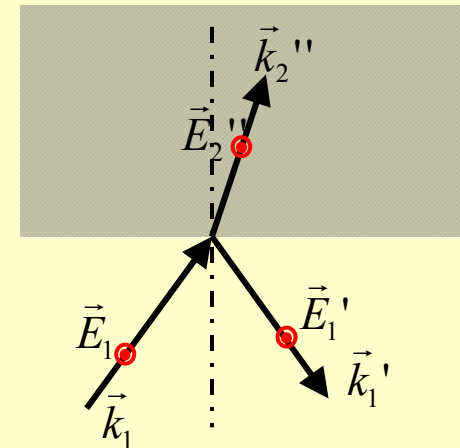
5、(半无限大绝缘介质分界面上)全反射现象

反射波的电场与入射波电场之比：

$$\frac{E_{0\perp}'}{E_{0\perp}} = \frac{\sqrt{\varepsilon_1} \cos \theta - \sqrt{\varepsilon_2} \cos \theta''}{\sqrt{\varepsilon_1} \cos \theta + \sqrt{\varepsilon_2} \cos \theta''}$$

电场沿着相同方向振动，因此
比值即代表了方向

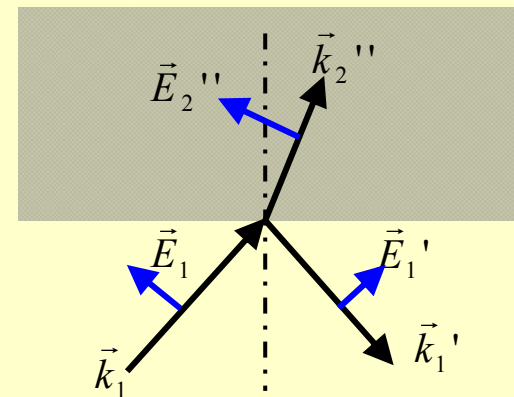
s 偏振 (\vec{E}_\perp)



$$\frac{E_{0\parallel}'}{E_{0\parallel}} = \frac{\sqrt{\varepsilon_2} \cos \theta - \sqrt{\varepsilon_1} \cos \theta''}{\sqrt{\varepsilon_2} \cos \theta + \sqrt{\varepsilon_1} \cos \theta''}$$

一般情况下电场振动方向并不
相同，除非在垂直入射情形！

p 偏振 (\vec{E}_\parallel)

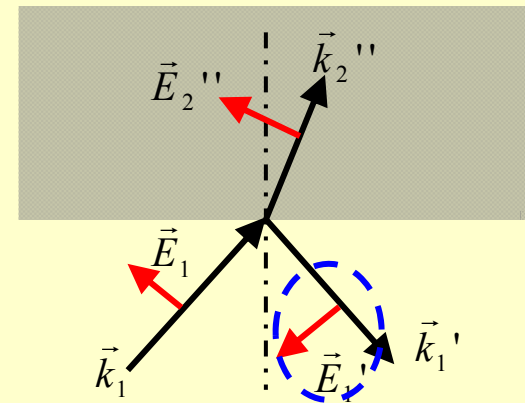
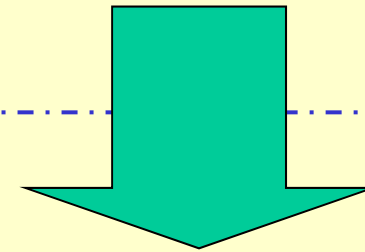
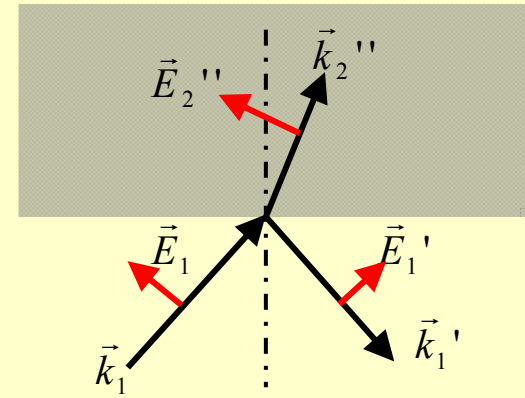


p 偏振:

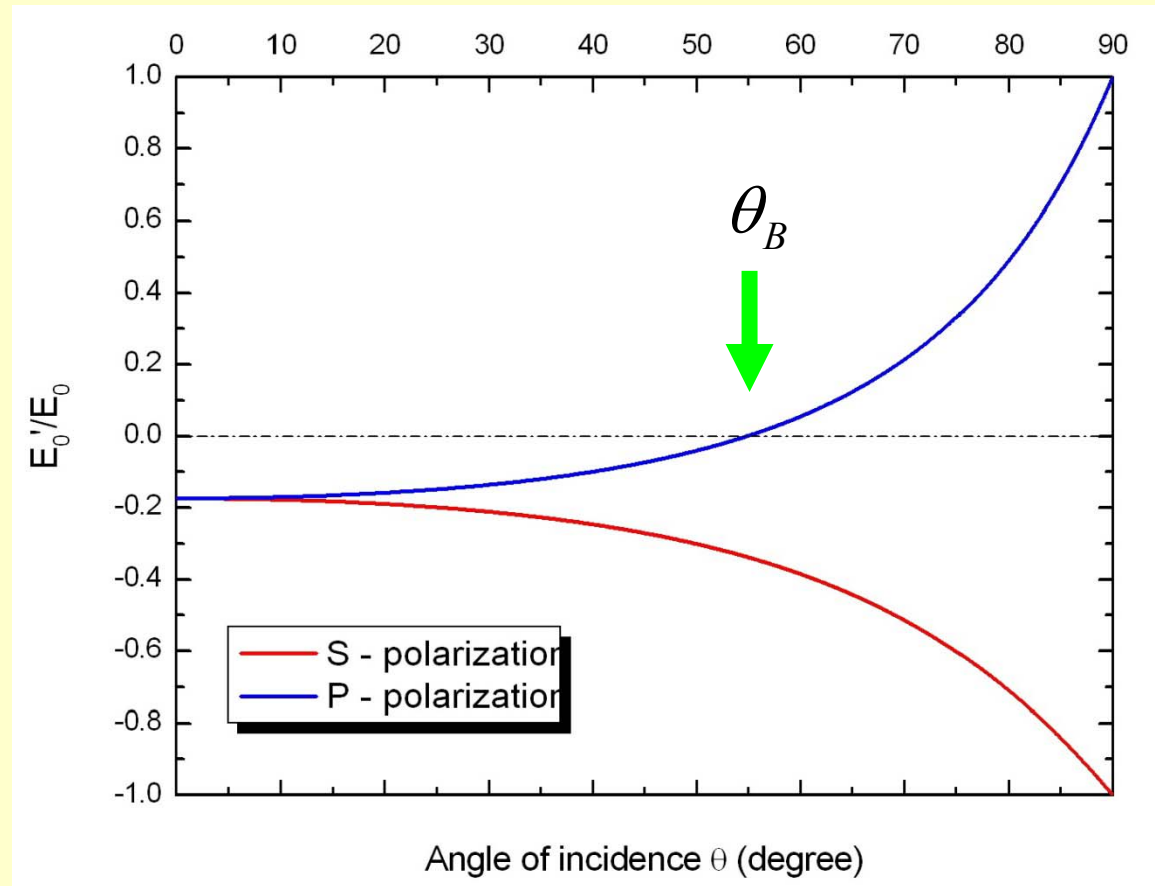
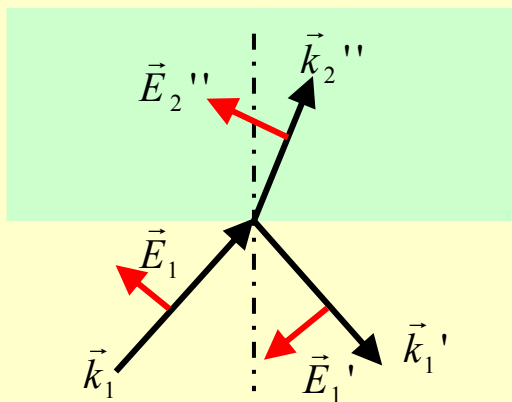
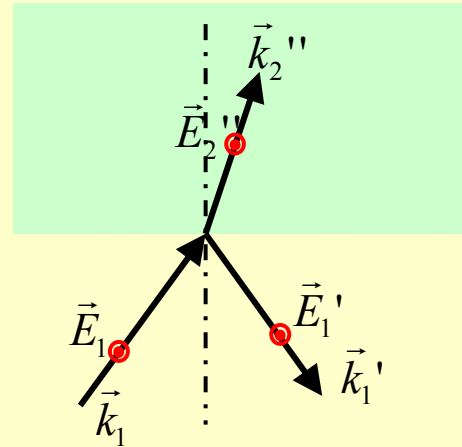
$$\frac{E_{0//}'}{E_{0//}} = \frac{\sqrt{\varepsilon_2} \cos \theta - \sqrt{\varepsilon_1} \cos \theta''}{\sqrt{\varepsilon_2} \cos \theta + \sqrt{\varepsilon_1} \cos \theta''}$$

但按照图示，在垂直入射下，
比值为正，表示的是方向相反！

$$\frac{E_{0//}'}{E_{0//}} = \ominus \frac{\sqrt{\varepsilon_2} \cos \theta - \sqrt{\varepsilon_1} \cos \theta''}{\sqrt{\varepsilon_2} \cos \theta + \sqrt{\varepsilon_1} \cos \theta''}$$



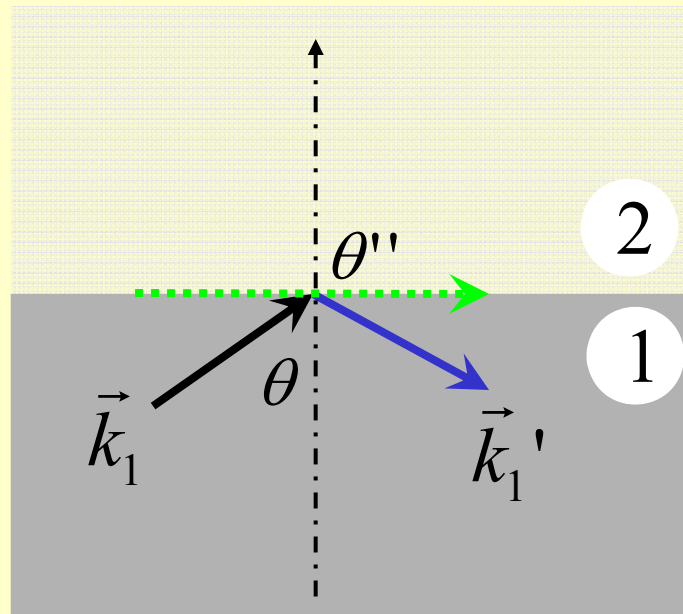
1) 假设: $n_1 = 1.00$, $n_2 = 1.42$ ($n_1 < n_2$)



- 此时, 对于s 偏振, 反射波的电场与入射波的电场始终反向——电磁波反射过程中的半波损失。

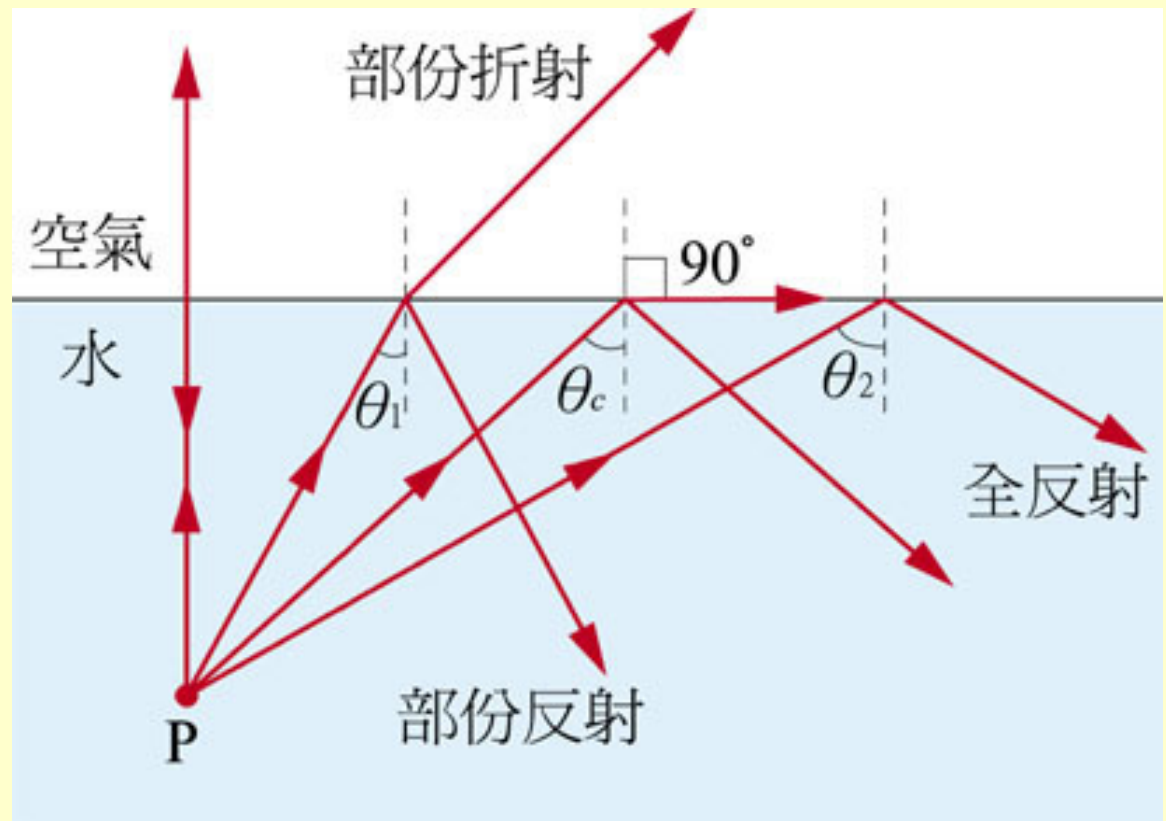
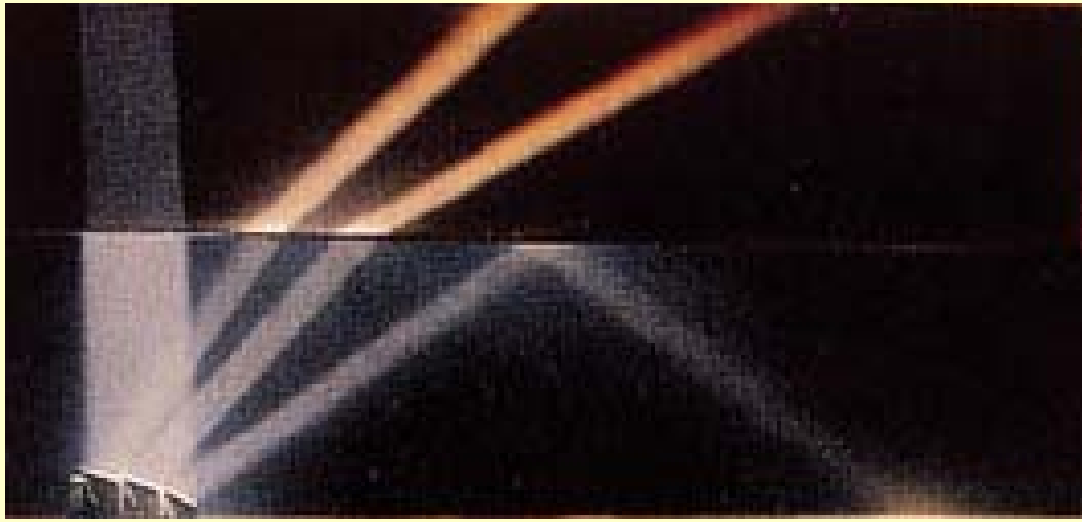
$$n_1 \sin \theta = n_2 \sin \theta''$$

2) 假设：电磁波从折射率**高**的介质（光子能量低）入射到折射率**低**（光子能量高）的介质分界面（会发生**全反射现象**）

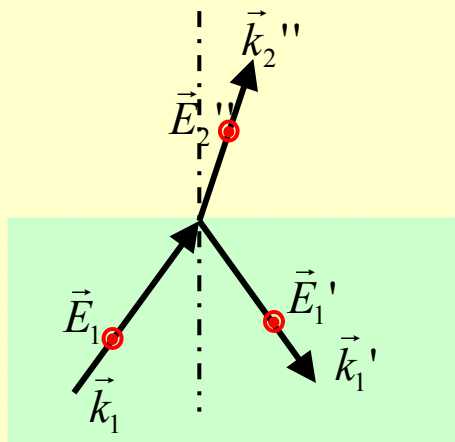


$$(n_2 < n_1)$$

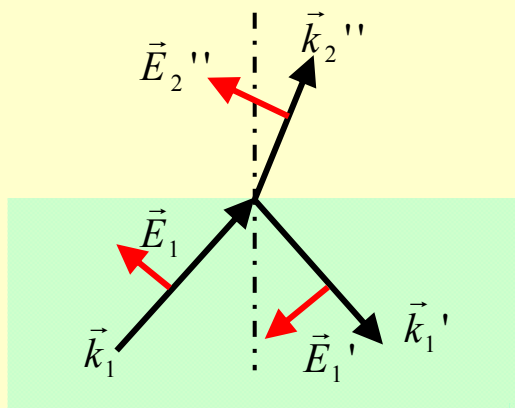
假设： $n_1 = 1.42$, $n_2 = 1.00$



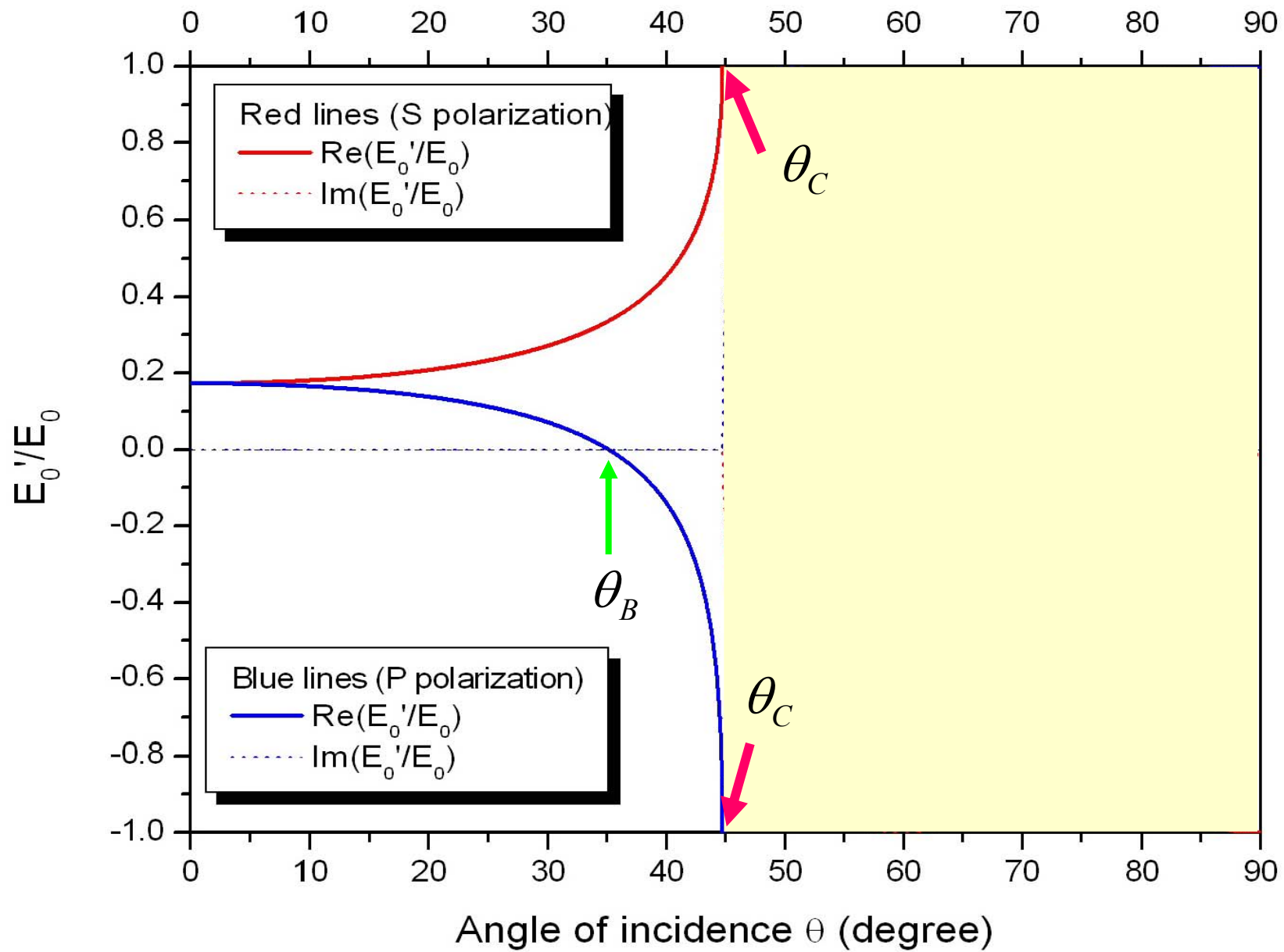
假设： $n_1 = 1.42, n_2 = 1.00$

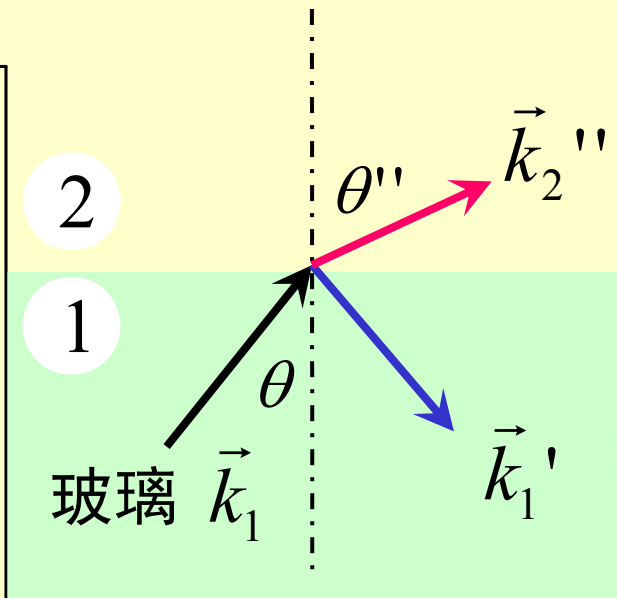
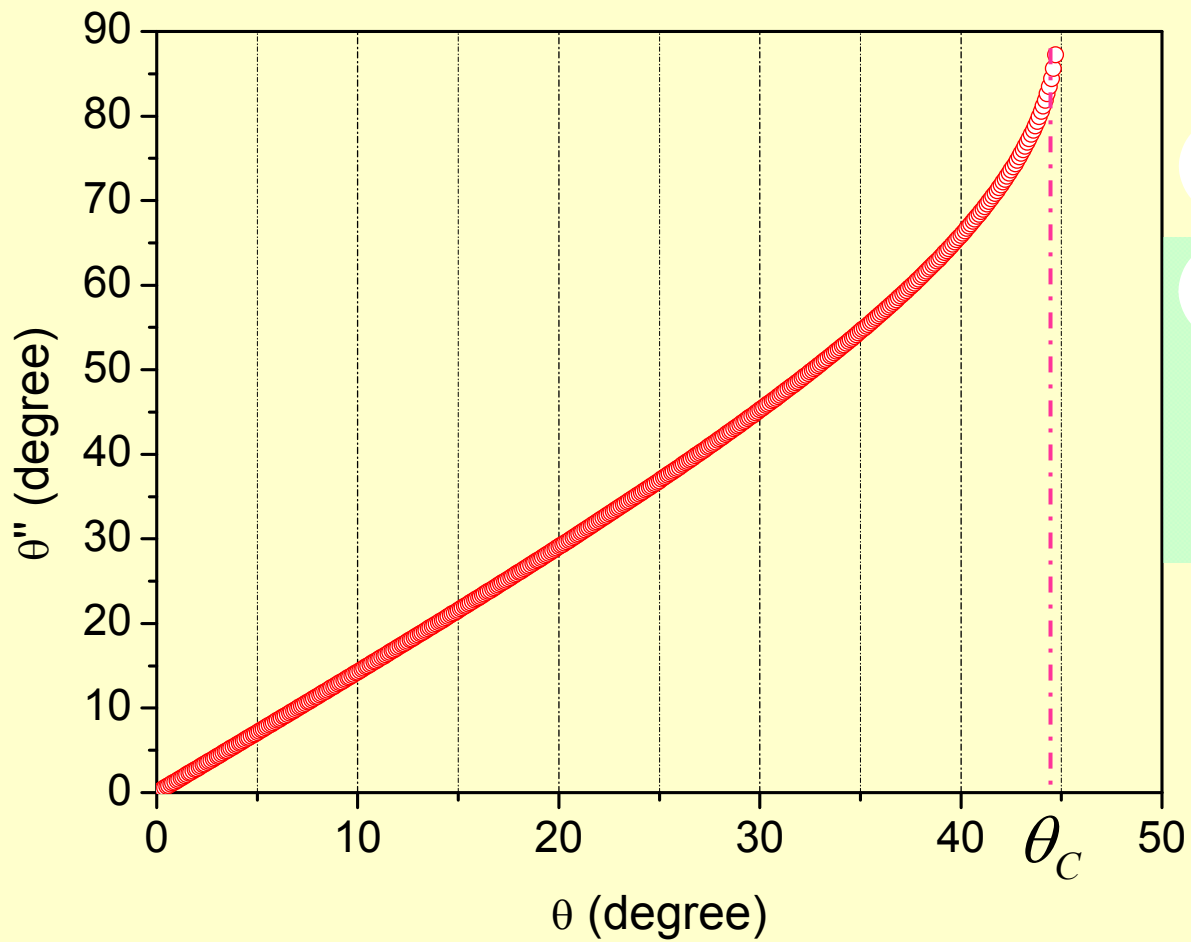


$$\frac{E_{0\perp}'}{E_{0\perp}} = \frac{\sqrt{\epsilon_1} \cos \theta - \sqrt{\epsilon_2} \cos \theta''}{\sqrt{\epsilon_1} \cos \theta + \sqrt{\epsilon_2} \cos \theta''}$$



$$\frac{E_{0\parallel}'}{E_{0\parallel}} = -\frac{\sqrt{\epsilon_2} \cos \theta - \sqrt{\epsilon_1} \cos \theta''}{\sqrt{\epsilon_2} \cos \theta + \sqrt{\epsilon_1} \cos \theta''}$$

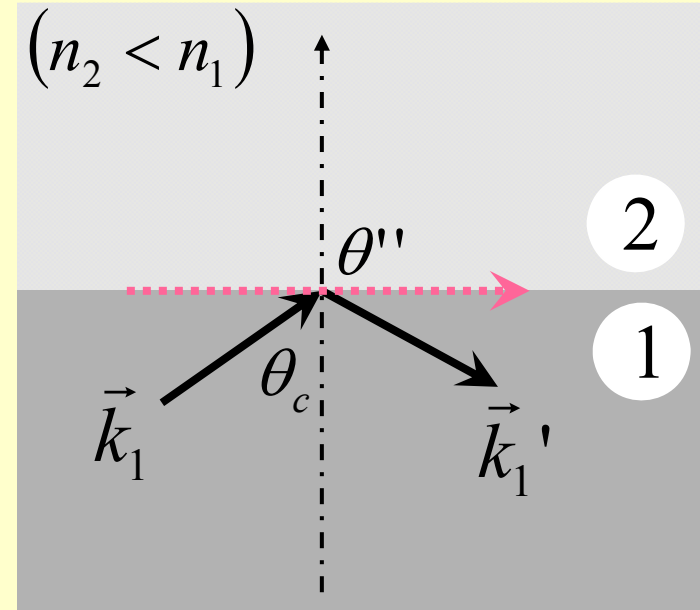




发现：当 $\theta = \theta_c$ 时， $\theta'' = 90^\circ$

1) 定义临界（入射）角：

$$\sin \theta_c = n_{21}$$



$$n_1 \sin \theta = n_2 \sin \theta''$$

① 当 $\theta > \theta_c$ 时, $\sin \theta'' > 1$

② 在 $\theta > \theta_c$ 时, θ'' 已失去它作为几何上的解释。

2) 全反射情况下的反射波

$$n_2 \sin \theta'' = n_1 \sin \theta$$

当 $\theta > \theta_c$ 时, $\sin \theta'' > 1$

→ $\sin \theta'' = \sin \theta / n_{21} (> 1)$

$$\cos \theta'' = \sqrt{1 - \sin^2 \theta''}$$

$$= i \sqrt{\left(\frac{\sin \theta}{n_{21}}\right)^2 - 1}$$

$$\frac{E_{0\perp}'}{E_{0\perp}} = \frac{\sqrt{\varepsilon_1} \cos \theta - \sqrt{\varepsilon_2} \cos \theta''}{\sqrt{\varepsilon_1} \cos \theta + \sqrt{\varepsilon_2} \cos \theta''}$$

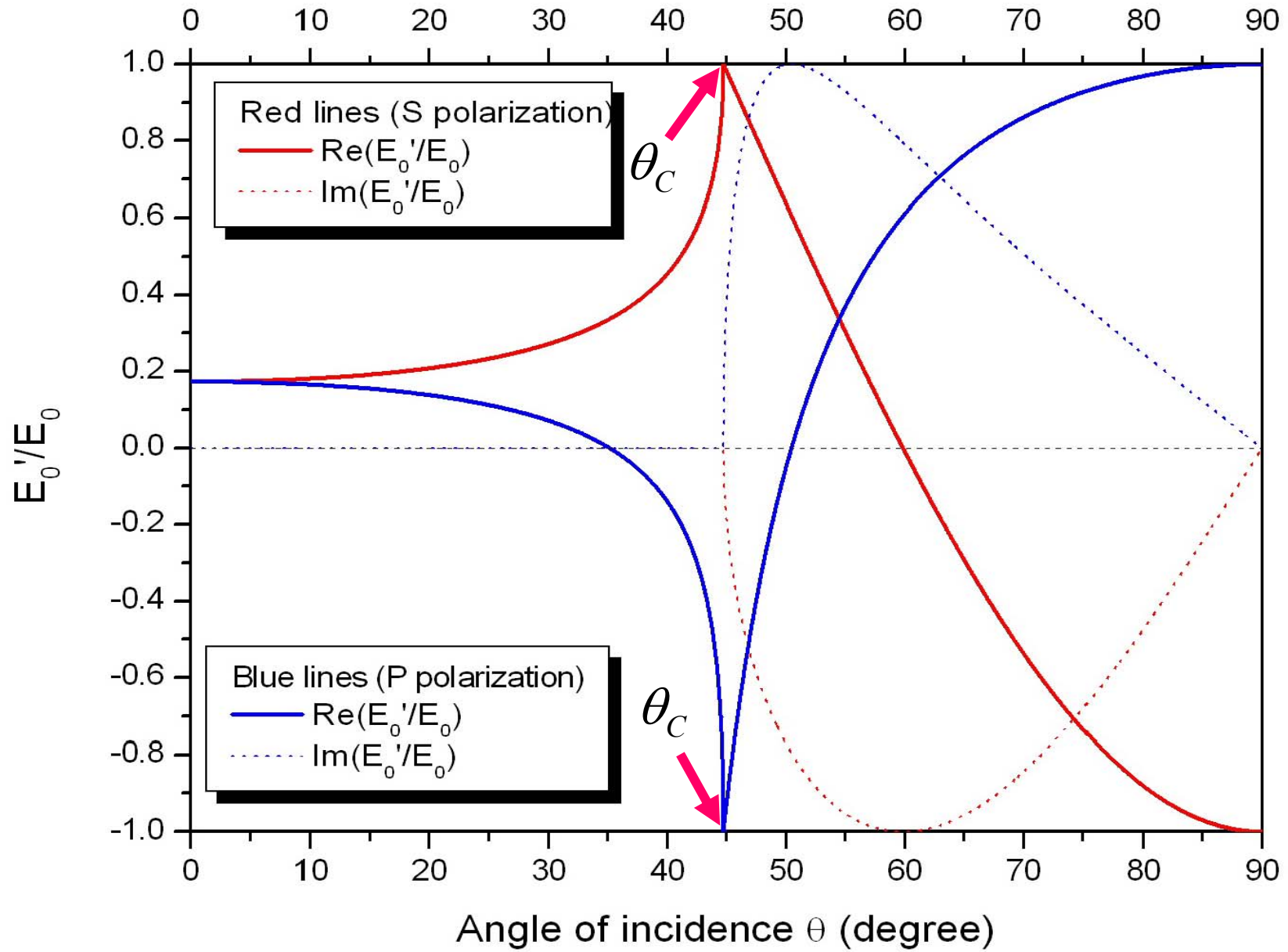
$$\frac{E_{0//}'}{E_{0//}} = -\frac{n_2 \cos \theta - n_1 \cos \theta''}{n_2 \cos \theta + n_1 \cos \theta''}$$



$$\frac{E_{0\perp}'}{E_{0\perp}} = \frac{\cos \theta - i \sqrt{\sin^2 \theta - n_{21}^2}}{\cos \theta + i \sqrt{\sin^2 \theta - n_{21}^2}}$$

$$\frac{E_{0//}'}{E_{0//}} = -\frac{n_{21}^2 \cos \theta - i \sqrt{\sin^2 \theta - n_{21}^2}}{n_{21}^2 \cos \theta + i \sqrt{\sin^2 \theta - n_{21}^2}}$$

Both complex beyond the critical angle !



$$\frac{E_{0\perp}'}{E_{0\perp}} = \frac{\cos \theta - i\sqrt{\sin^2 \theta - n_{21}^2}}{\cos \theta + i\sqrt{\sin^2 \theta - n_{21}^2}}$$

$$\frac{E_{0//}'}{E_{0//}} = \frac{n_{21}^2 \cos \theta - i\sqrt{\sin^2 \theta - n_{21}^2}}{n_{21}^2 \cos \theta + i\sqrt{\sin^2 \theta - n_{21}^2}}$$

容易验证：当 $\theta > \theta_c$ 时，

$$\left| \frac{E_{0\perp}'}{E_{0\perp}} \right| = 1$$

$$\left| \frac{E_{0//}'}{E_{0//}} \right| = 1$$

在全反射条件下：

- ① 对于**任意偏振**，都在同一个角度开始发生全反射；
- ② 反射波与入射波具有相同的振幅，但存在一定的位相差；
- ③ 反射波的平均能流密度等于**入射波的平均能流密度**。

3) 全反射情况的折射波

全反射时的折射波成是沿着界面传播的**表面波**

$$k_{2z}'' = \sqrt{k_2^2 - k_{2x}^2} = \sqrt{k_2^2 - k_2^2 \sin^2 \theta''} = k_2 \sqrt{1 - \sin^2 \theta''}$$

$$k_{2z}'' = i\kappa$$

$$\vec{E}''(\vec{x}, t) = \vec{E}_0'' \exp\left[i(\vec{k}_2'' \cdot \vec{x} - \omega'' t)\right]$$



$$\vec{k}_2'' \cdot \vec{x} = k_{2x}'' x + k_{2z}'' z = k_{2x}'' x + i\kappa \cdot z$$

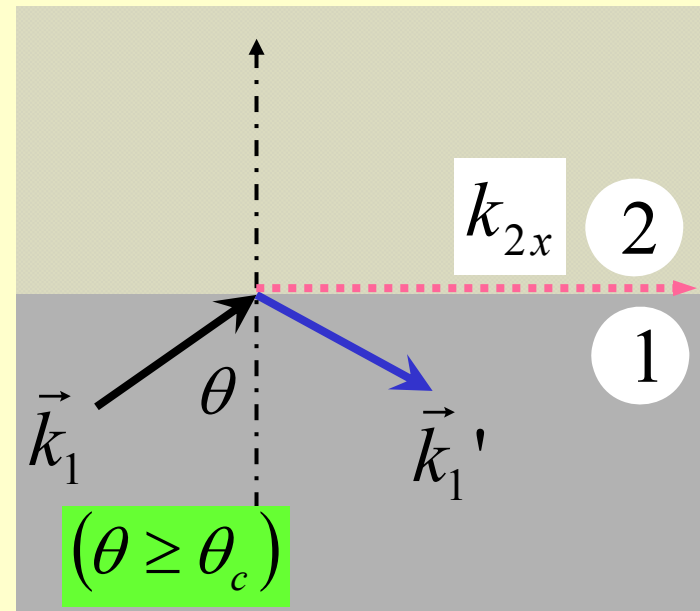
$$\vec{E}''(\vec{x}, t) = \vec{E}_0'' \exp(-\kappa z) \exp[i(k_{2x}'' x - \omega t)]$$

$$\vec{E}''(\vec{x}, t) = \vec{E}_0'' e^{-\kappa z} e^{i(k_{2x}'' x - \omega t)}$$

① 介质 2 中的折射波数：

$$k_2''/n_2 = k_1/n_1$$

$$k_2'' = \frac{n_2}{n_1} k_1 = n_{21} k_1$$



② 在全反射的情况下，波矢分量边值关系仍然成立

$$k_{2x}'' = k_{1x} = k_1 \sin \theta$$

$$k_2'' = n_{21} k_1$$

③ 全反射的折射波矢 z 分量:

$$k_{2x}'' = k_{1x} = k_1 \sin \theta$$

$$\rightarrow k_{2z}'' = \sqrt{(k_2'')^2 - (k_{2x}'')^2}$$

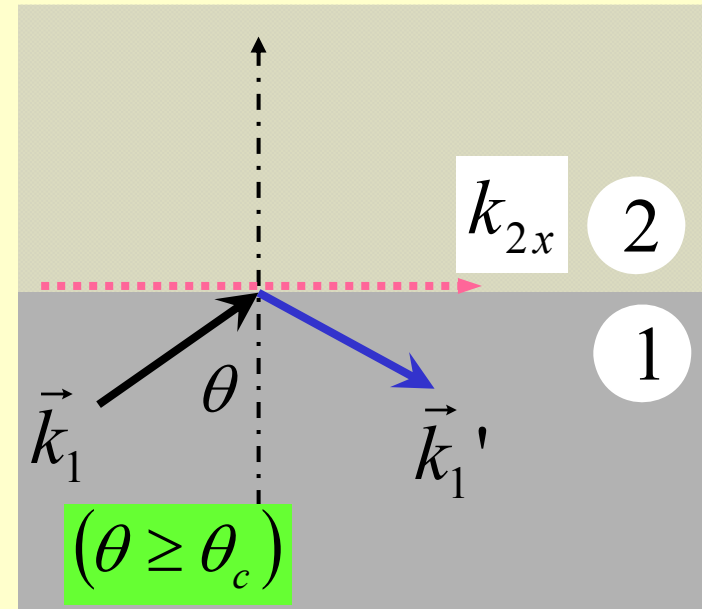
$$= \sqrt{k_1^2 n_{21}^2 - k_1^2 \sin^2 \theta}$$

$$= i k_1 \sqrt{\sin^2 \theta - n_{21}^2}$$

(一个纯虚数)

定义: $k_{2z}'' = i\kappa$

$$\kappa = k_1 \sqrt{\sin^2 \theta - n_{21}^2}$$



④ 全反射时折射波—表面波

$$k_{2z}'' = i\kappa \quad \kappa = k_1 \sqrt{\sin^2 \theta - n_{21}^2}$$

$$\vec{E}''(\vec{x}, t) = \vec{E}_0'' \exp[i(\vec{k}_2'' \cdot \vec{x} - \omega'' t)]$$

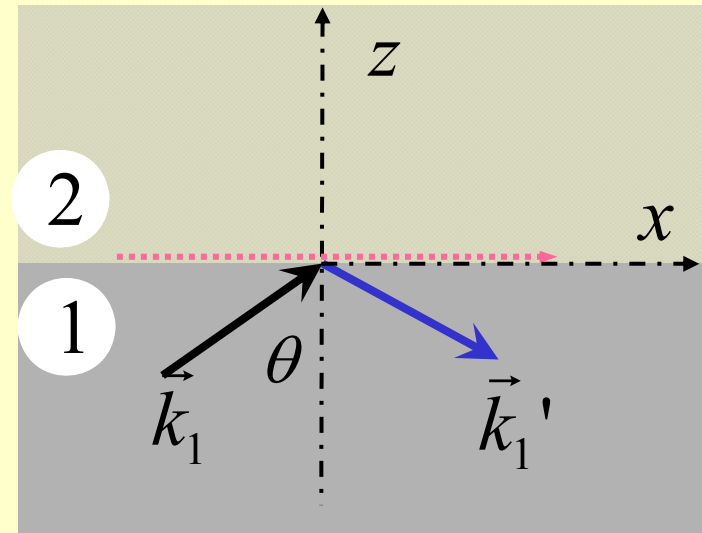
$$\vec{k}_2'' \cdot \vec{x} = k_{2x}'' x + k_{2z}'' z = k_{2x}'' x + i\kappa \cdot z$$

$$\vec{E}''(\vec{x}, t) = \vec{E}_0'' \exp(-\kappa z) \exp[i(k_{2x}'' x - \omega t)]$$

$$\vec{E}''(\vec{x}, t) = \vec{E}_0'' e^{-\kappa z} e^{i(k_{2x}'' x - \omega t)}$$

$$\vec{E}''(\vec{x}, t)$$

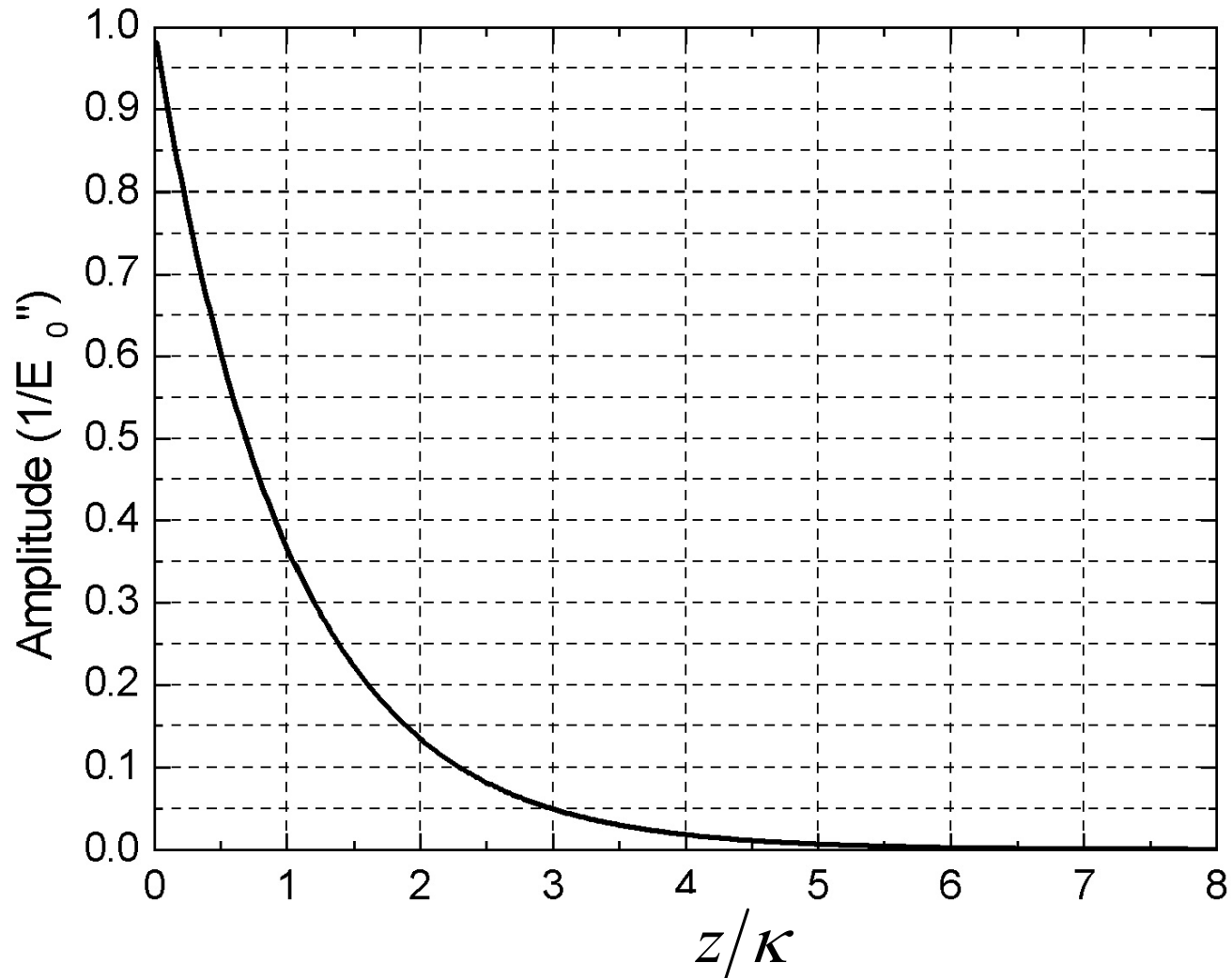
$$= \vec{E}_0'' e^{-\kappa z} e^{i(k_{2x}'' x - \omega t)}$$



$$(\theta \geq \theta_c)$$

- 它表示沿 x 方向传播、振幅沿 z 轴衰减的时谐波；
- 这种时谐波只存在于界面附近一薄层内，该薄层的厚度在 $1 \sim 2$ 个 λ 的线度内。
- 全反射时的折射波为**表面波**。

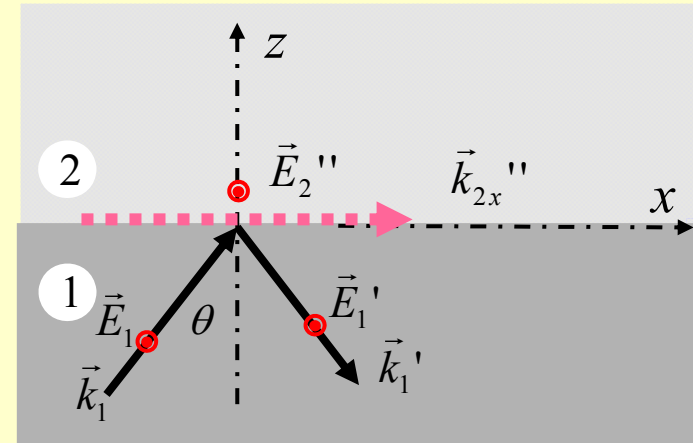
$$\vec{E}''(\vec{x}, t) = \vec{E}_0'' \exp(-\kappa z) \exp[i(k_{2x}'' x - \omega t)]$$



4) 折射波的能量密度

$$(\vec{S} = \vec{E} \times \vec{H})$$

假设入射波的电场垂直于入射面，即S偏振情形



介质 2 中的能流密度：

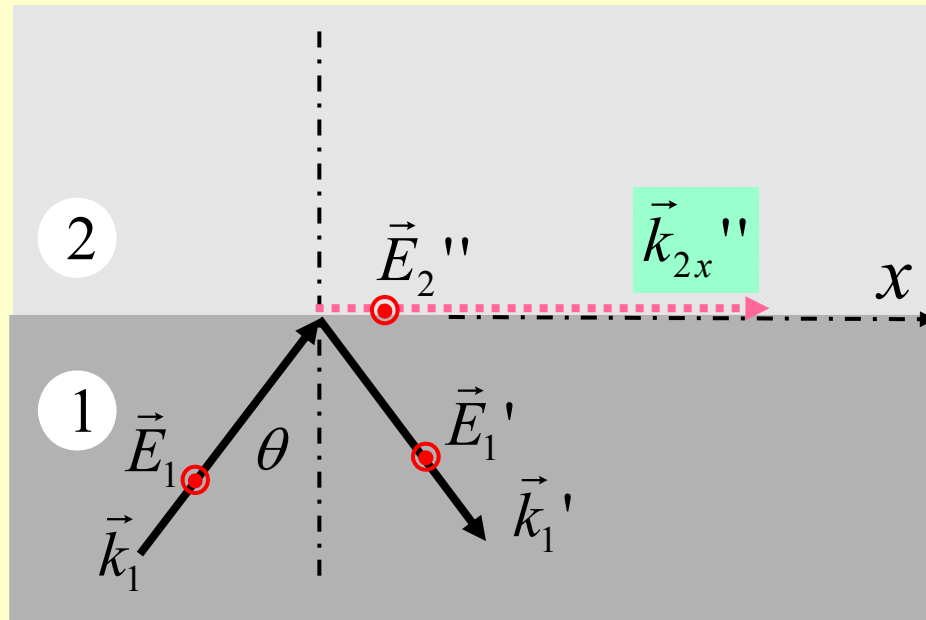
$$\boxed{(\vec{S} = \vec{E} \times \vec{H})}$$

$$S_{2x} = E_2'' H_{2z} = \frac{1}{\mu_2} \underline{E_2''} \underline{B_{2z}''}$$

须各取其实部

$$S_{2z} = \ominus E_2'' H_{2x} = -\frac{1}{\mu_2} \underline{E_2''} \underline{B_{2x}''}$$

对于S偏振情形：



$$\vec{B} = (1/\omega)\vec{k} \times \vec{E}$$

$$\vec{k}_2'' = (k_{2x}'', 0, k_{2z}'')$$

$$\vec{E}'' = (0, E'', 0)$$

折射波：
$$\vec{E}''(\vec{x}, t) = (E_0'' e^{-\kappa z}) e^{i(k_{2x}'' x - \omega t)} \vec{e}_y$$

$$\vec{E}''(\vec{x}, t) = (E_0'' e^{-\kappa z}) e^{i(k_{2x}'' x - \omega t)} \vec{e}_y$$

$$\vec{B} = (1/\omega) \vec{k} \times \vec{E}$$

$$\left\{ \begin{array}{l} B_{2z}'' = \frac{1}{\omega} k_{2x}'' E_2'' \\ B_{2x}'' = -\frac{1}{\omega} k_{2z}'' E_2'' \end{array} \right.$$

$$B_{2z}'' = \frac{k_2'' \sin \theta}{\omega n_{21}} E_2''$$

$$= \sqrt{\mu_2 \epsilon_2} \frac{\sin \theta}{n_{21}} E_2''$$

$$\vec{k}_2'' = (k_{2x}'', 0, k_{2z}'')$$

$$\vec{E}'' = (0, E'', 0)$$

$$k_2'' = \omega \sqrt{\mu_2 \epsilon_2}$$

$$k_{2x}'' = k_1 \sin \theta$$

$$k_2'' = n_{21} k_1$$

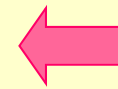
$$B_{2z}'' = \sqrt{\mu_2 \epsilon_2} \frac{\sin \theta}{n_{21}} E_2''$$

$$B_{2x}'' = -\frac{1}{\omega} k_{2z}'' E_2''$$

$$k_{2z}'' = ik_1 \sqrt{\sin^2 \theta - n_{21}^2}$$

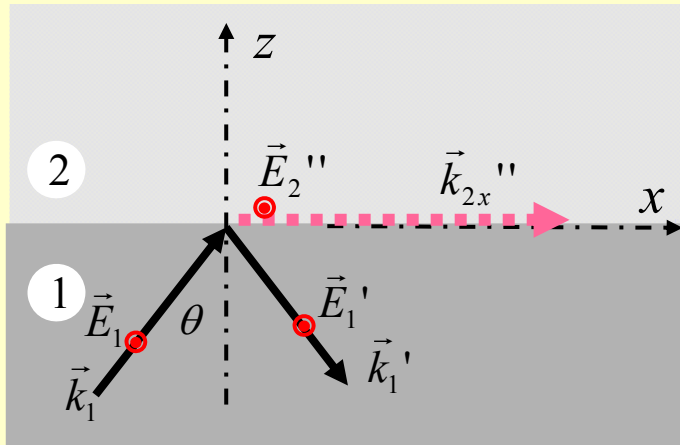
$$B_{2x}'' = -i \frac{1}{\omega} k_1 \sqrt{\sin^2 \theta - n_{21}^2} E_2''$$

$$= -i \frac{k_1 n_{21}}{\omega} \sqrt{\left(\frac{\sin^2 \theta}{n_{21}^2} - 1 \right)} E_2''$$



$$k_2''/n_2 = k_1/n_1$$

$$= -i \frac{k_2''}{\omega} \sqrt{\left(\frac{\sin^2 \theta}{n_{21}^2} - 1 \right)} E_2''$$



$$\vec{E}''(\vec{x}, t) = (E_0'' e^{-\kappa z}) e^{i(k_{2x}'' x - \omega t)} \vec{e}_y$$

$$B_{2x}'' = -i \frac{k_2''}{\omega} \sqrt{\frac{\sin^2 \theta}{n_{21}^2} - 1} E_2''$$

$$B_{2z}'' = \sqrt{\mu_2 \epsilon_2} \frac{\sin \theta}{n_{21}} E_2''$$

介质 2 中的能流密度：($\vec{S} = \vec{E} \times \vec{H}$)

$$S_{2x} = E_2'' H_{2z} = \frac{1}{\mu_2} \underline{E_2''} \underline{B_{2z}''}$$

$$S_{2z} = -E_2'' H_{2x} = -\frac{1}{\mu_2} \underline{E_2''} \underline{B_{2x}''}$$

$$\operatorname{Re}(B_{2z}''') = \sqrt{\mu_2 \varepsilon_2} \frac{\sin \theta}{n_{21}} \operatorname{Re}(E_2''')$$

$$\operatorname{Re}(B_{2x}''') = \frac{k_{2x}'''}{\omega} \sqrt{\frac{\sin^2 \theta}{n_{21}^2} - 1} \operatorname{Im}(E_2''')$$

$$B_{2z}'' = \sqrt{\mu_2 \varepsilon_2} \frac{\sin \theta}{n_{21}} E_2''$$

$$B_{2x}'' = -i \frac{k_{2x}''}{\omega} \sqrt{\frac{\sin^2 \theta}{n_{21}^2} - 1} E_2''$$

$$\vec{E}''(\vec{x}, t) = (E_0'' e^{-\kappa z}) e^{i(k_{2x}'' x - \omega t)} \vec{e}_y$$

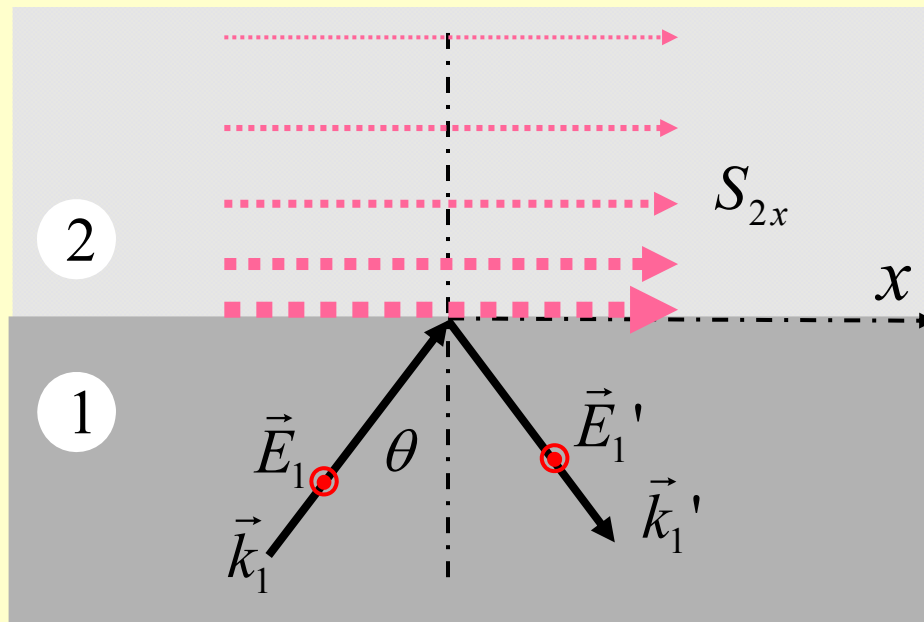
$$S_{2x} = \frac{1}{\mu_2} \operatorname{Re}(E_2''') \cdot \operatorname{Re}(B_{2z}''') = \frac{1}{\mu_2} \sqrt{\mu_2 \varepsilon_2} \frac{\sin \theta}{n_{21}} (\operatorname{Re} E_2''')^2$$

$$= \sqrt{\frac{\varepsilon_2}{\mu_2}} \frac{\sin \theta}{n_{21}} (E_0'')^2 e^{-2\kappa z} \cos^2(k_{2x}'' x - \omega t)$$

$$= \frac{1}{2} \sqrt{\frac{\varepsilon_2}{\mu_2}} \frac{\sin \theta}{n_{21}} (E_0'')^2 e^{-2\kappa z} \{1 + \cos[2(k_{2x}'' x - \omega t)]\}$$

$$S_{2x} = \frac{1}{2} \sqrt{\frac{\epsilon_2}{\mu_2}} \frac{\sin \theta}{n_{21}} (E_0'')^2 e^{-2\kappa z} \{1 + \cos[2(k_{2x}'' x - \omega t)]\}$$

$$\langle S_{2x} \rangle = \frac{1}{2} \sqrt{\frac{\epsilon_2}{\mu_2}} \frac{\sin \theta}{n_{21}} (E_0'')^2 e^{-2\kappa z}$$



$$\vec{E}''(\vec{x}, t) = (E_0'' e^{-\kappa z}) e^{i(k_{2x}'' x - \omega t)} \vec{e}_y$$

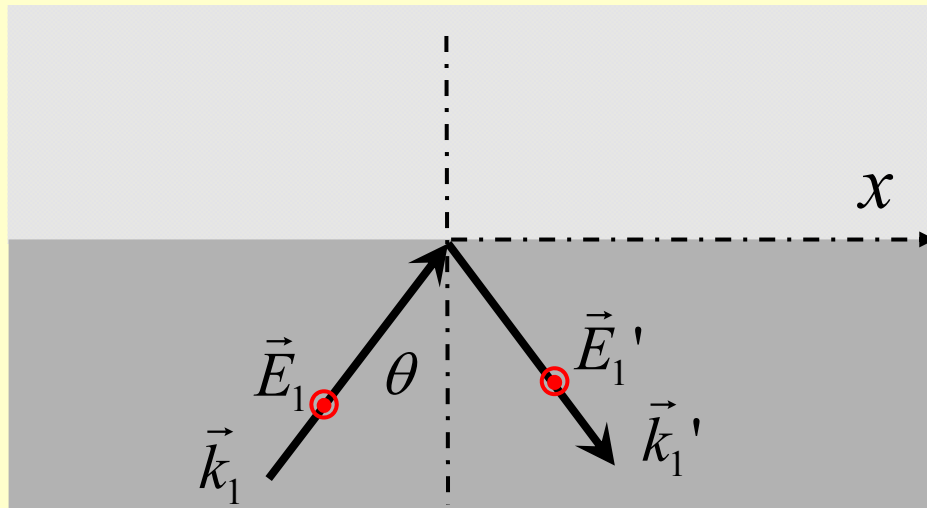
$$\text{Re}(B_{2x}'') = \frac{k_2''}{\omega} \sqrt{\frac{\sin^2 \theta}{n_{21}^2} - 1} \text{Im}(E_2'')$$

沿 z 轴的能流

$$S_{2z} = -(1/\mu_2) \text{Re}(E_2'') \text{Re}(B_{2x}'')$$

$$= -\frac{1}{\mu_2} \frac{k_2''}{\omega} \left(\frac{\sin^2 \theta}{n_{21}^2} - 1 \right)^{1/2} e^{-2\kappa z} (E_0'')^2 \\ \cdot \sin(k_{2x}'' x - \omega t) \cos(k_{2x}'' x - \omega t)$$

$$= -\frac{k_2''}{2\mu_2\omega} (E_0'')^2 e^{-2\kappa z} \left(\frac{\sin^2 \theta}{n_{21}^2} - 1 \right)^{1/2} \cdot \sin[2(k_{2x}'' x - \omega t)]$$

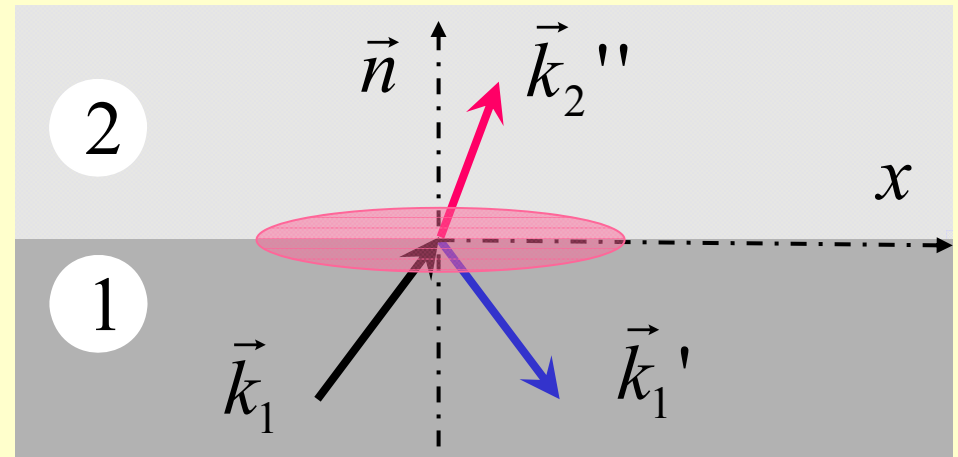


$$S_{2z} = -\frac{k_2''}{2\mu_2\omega} (E_0'')^2 e^{-2\kappa z} \left(\frac{\sin^2 \theta}{n_{21}^2} - 1 \right)^{1/2} \cdot \sin[2(k_{2x}'' x - \omega t)]$$

沿 z 轴能流在一个周期内的平均值：

$$\langle S_{2z} \rangle = 0$$

3) 反射系数:



$$R = \frac{\langle \vec{S}' \rangle \cdot \vec{n}}{\langle \vec{S} \rangle \cdot \vec{n}} = \frac{|E_0'|^2 \vec{e}_{k'} \cdot \vec{n}}{|E_0|^2 \vec{e}_k \cdot \vec{n}} = \frac{|E_0'|^2}{|E_0|^2}$$

4) 折射系数:

$$T = \frac{\langle \vec{S}'' \rangle \cdot \vec{n}}{\langle \vec{S} \rangle \cdot \vec{n}} = \frac{n_2 |E_0''|^2 \vec{e}_{k''} \cdot \vec{n}}{n_1 |E_0|^2 \vec{e}_k \cdot \vec{n}} = \frac{n_2 |E_0''|^2 \cos \theta''}{n_1 |E_0|^2 \cos \theta}$$

在全反射条件下，

- ① 折射波介质 2 的**存在沿着表面传播的折射波**，因此存在能流；
- ② **平均能流密度**存在沿分界面的分量；
- ③ 而沿面法线方向而透入第二介质的**平均能流密度**为零。

作业

第四章：习题3

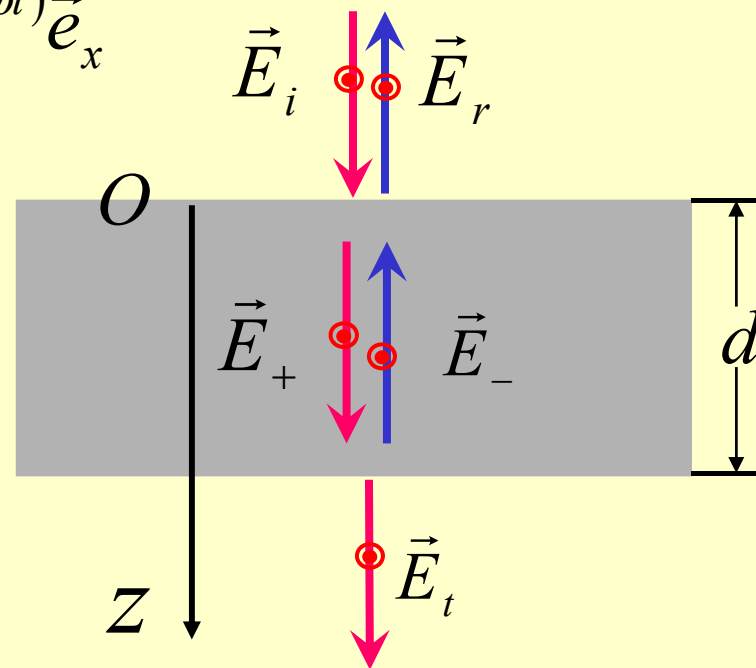
思考题：单色平面电磁波垂直入射到一介质膜上，在入射区，存在入射和反射波；在介质膜内，存在前向和反向波；在透射区存在透射波，分别表示为

$$\vec{E}_i = E_{i0} e^{i(kz - \omega t)} \vec{e}_x, \quad \vec{E}_r = E_{r0} e^{i(-kz - \omega t)} \vec{e}_x$$

$$\vec{E}_+ = E_{+0} e^{i(k_m z - \omega t)} \vec{e}_x$$

$$\vec{E}_- = E_{-0} e^{i(-k_m z - \omega t)} \vec{e}_x$$

$$\vec{E}_t = E_{t0} e^{i(kz - \omega t)} \vec{e}_x$$



试根据介质分界面处电磁场边界条件，写出上述电场振幅之间的关系。